

## Research Article

# Development of a Real-Time, Large Area, High Spatial Resolution Particle Tracker Based on Scintillating Fibers

**D. Lo Presti,<sup>1,2</sup> D. L. Bonanno,<sup>1</sup> F. Longhitano,<sup>2</sup> C. Pugliatti,<sup>1,2</sup> S. Aiello,<sup>2</sup> G. A. P. Cirrone,<sup>3</sup> V. Giordano,<sup>2</sup> E. Leonora,<sup>2</sup> N. Randazzo,<sup>2</sup> S. Reito,<sup>2</sup> F. Romano,<sup>3</sup> G. V. Russo,<sup>1,2</sup> M. Russo,<sup>1,2</sup> V. Sipala,<sup>4,5</sup> C. Stancampiano,<sup>2</sup> and C. Ventura<sup>2</sup>**

<sup>1</sup> Department of Physics and Astronomy, University of Catania, 95123 Catania, Italy

<sup>2</sup> Istituto Nazionale di Fisica Nucleare (INFN), 95123 Catania, Italy

<sup>3</sup> Laboratori Nazionali del Sud (LNS), 95123 Catania, Italy

<sup>4</sup> University of Sassari, 07100 Sassari, Italy

<sup>5</sup> Istituto Nazionale di Fisica Nucleare (INFN), Sezione di Cagliari, 09042 Monserrato, Italy

Correspondence should be addressed to D. Lo Presti; [domenico.lopresti@ct.infn.it](mailto:domenico.lopresti@ct.infn.it)

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The design of a detector for tracking charged particles is presented together with the characterization techniques developed to extract the main design specifications. The goals for the final detector are to achieve real-time imaging performances, a large detection area, and a high spatial resolution, particularly suitable for medical imaging applications. This paper describes the prototype of the tracker plane, which has a  $20 \times 20 \text{ cm}^2$  sensitive area consisting of two crossed ribbons of  $500 \mu\text{m}$  square scintillating fibers. The information about the hit position extracted real-time tracker in an innovative way, using a reduced number of the read-out channels to obtain a very large detection area but with moderate costs and complexity. The performances of the tracker have been investigated using  $\beta$  sources, cosmic rays, and a 62 MeV proton beam.

## 1. Introduction

Cutting edge research in the treatment of tumors has been oriented towards hadrontherapy, one of the most effective external radiotherapy techniques, which uses charged particle beams (protons and carbon ions) with energy up to 400 AMeV. Such beams make it possible to accurately release the dose required to control a cancerous mass, leaving at the same time the surrounding healthy tissue almost untouched. The maximum advantage from using charged particle beams is reached when there is precise information regarding the stopping power of the particles used for the radiotherapy treatments. The direct use of this information, rather than that from X-ray tomography, leads to a more accurate evaluation of the distribution of the dose and can be used to verify the positioning of the patient.

Therefore, the availability of very accurate imaging systems is of fundamental importance [1]. Our task is to design and build an imaging system for charged particles based on

the consolidated principle of residual range measurement [2] taking, at the same time, advantage of new detection techniques. The aim is to use this system to achieve large detection areas (up to  $30 \times 30 \text{ cm}^2$ ) suitable for almost all medical physics applications, high spatial resolution (up to 150 microns) and time resolution (up to 2 ns). With this in mind, we have developed a prototype of an X-Y tracker plane, the OFFSET detector, mainly funded by the Istituto Nazionale di Fisica Nucleare (INFN), which has been accurately tested with radioactive sources, cosmic rays, and the 62 MeV proton beam available at the Laboratori Nazionali del Sud (LNS) CATANA proton therapy facility.

## 2. OFFSET

The OFFSET X-Y detector consists of two planes of scintillating fibers (Sci-Fi) orthogonal to each other. The  $20 \times 20 \text{ cm}^2$  sensitive area of the prototype was built employing

500  $\mu\text{m}$  square multicladding BCF-12 [3] Sci-Fi manufactured by Saint-Gobain. In these fibers, the energy released by a crossing particle produces an isotropic emission of light. Only a part of this light is channeled into the fiber [4], which at this point acts as a guide. This light flows in both directions along the fiber. The factory can deliver the fibers as a preglued, aligned, 400 fiber ribbons. We have arranged two ribbons into orthogonal layers, one above the other, kept in position by the pressure of two square aluminum frames, delimiting the sensitive area of the detector, as shown in Figure 1. In a classical read-out scenario, every Sci-Fi must be optically coupled to a light sensor, each read, from a channel of the front-end electronics. In the case of the  $20 \times 20 \text{ cm}^2$  prototype there are  $400 + 400$  channels, meaning that a suitable read-out system not only would be complex but also would certainly suffer from high dead times.

**2.1. Channel Reduction System.** The OFFSET tracker uses a system, for the reduction of the read-out channels, suitable for many imaging conditions. It detects one particle at a time. This architecture reduces the number of the read-out channels for a linear segmented detector and it is a modern version of previous applications [5, 6]. The operating principle of the channel reduction can be explained as follows. Let us consider a strip detector. Each strip is read from both ends but the meaning of the two signals is interpreted differently as a result of different groupings. At one end, the strips are read together in groups of  $n$  contiguous strips, while at the other end the first strips of each group are grouped in *StripSet* (SS) 1, the second strips of each group in SS 2, and so on. A particle crossing one strip generates two signals at both ends.

Then we have a signal from the  $i$ th group and another from the  $j$ th StripSet that uniquely identify the  $\text{Strip}_{\text{hit}}$ , hit by the particle according to

$$\text{Strip}_{\text{hit}} = (i - 1) * n + j. \quad (1)$$

The X-Y strip detector shown in Figure 2, consisting of 16 strips for each plane, is an example of a two-dimensional strip detector, where the channel reduction system is applied. In a classical read-out scenario of a two-dimensional strip detector, there would be 16 read-out channels for the X direction and 16 for the Y direction, making 32 channels. In the example the position of the impact point, marked with a star, is  $x = 11$  and  $y = 6$ . Figure 2 also shows the proposed read-out reduction system that allows the total number of channels to be reduced to only 16. Using a simple mathematical treatment the optimized number of channels appears to be equal to  $4\sqrt{N}$ , where  $N$  is the total number of strips per layer, X or Y. It is very interesting that, when  $N$  is large, the reduction factor becomes significant, especially in real-time applications.

The bound coincidence between the ends of each strip, not present in a simple strip read-out system, allows spurious signals (noise, crosstalk, dark current, etc.) to be automatically filtered. It should be noted that, to reconstruct the point where the particle crosses the detector (event), it is necessary for it to release energy in both planes. The application of a read-out channel reduction system consists in a suitable grouping and coupling of the Sci-Fi to larger standard (clear)

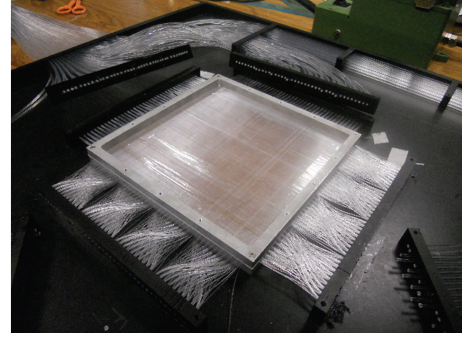


FIGURE 1: The OFFSET tracker without the cover. The  $20 \times 20 \text{ cm}^2$  sensitive area, delimited by the square frame, is visible.

optical fibers. Each group of  $n$  Sci-Fi is coupled to a suitable clear fiber that is faced to a light sensor. The read-out channel reduction factor depends only on the relationship between the cross-sections of the Sci-Fi and of the clear fibers. Figure 3 shows (a) the scheme of the optical coupling and (b) pictures of the Sci-Fi and clear fibers prepared for coupling.

In the OFFSET tracker, the application of the read-out channel reduction system led to 160 channels, exactly one-fifth of those necessary without channel reduction.

**2.2. Photosensor.** A single multianode photomultiplier (PSPM) is used as a light sensor instead of having separate light sensors for each clear fiber. We have chosen the  $16 \times 16$  pixels H9500 PSPM Hamamatsu photomultiplier [7]. It needs only one high voltage power supply and provides an additional signal, called the dynode, which is connected to all the last dynodes of each PSPM channel.

In the detector, 10 Sci-Fi are coupled to a single clear fiber. The light from the scintillating fibers propagates through the clear ones to the distance required, which in the case of the OFFSET tracker is about one meter, to reach the PSPM photocathode pixels. The coupling is made by routing and fixing the Sci-Fi and the clear fibers mechanically with optical gel. The size of the clear fibers is constrained by the pixel size of the selected photomultiplier, about  $2.8 \times 2.8 \text{ mm}^2$ , which limits the scale of reduction of the detector channels. Using photomultipliers with a larger pixel area or smaller Sci-Fi, the channel reduction could increase significantly.

**2.3. Front-End Electronics.** The front-end electronics is simple and very fast. The PSPM is socketed onto the front-end board. The anodic resistance for all channels was chosen as a compromise between the amplitude and the timing characteristics of the anodic voltage signal [8]. A fast comparator that feeds a monostable reads each of the 160 PSPM anodic signals. The threshold chosen for the comparators is about 1/3 of the mean amplitude of a single photoelectron.

**2.4. Data Acquisition.** The front-end electronics information is acquired by simple digital acquisition electronics for subsequent preanalysis, filtering, and fast storage into a PC. Logic signals from the front-end board are fed into a data acquisition module, a real-time FPGA PXI-7813R [9], via four

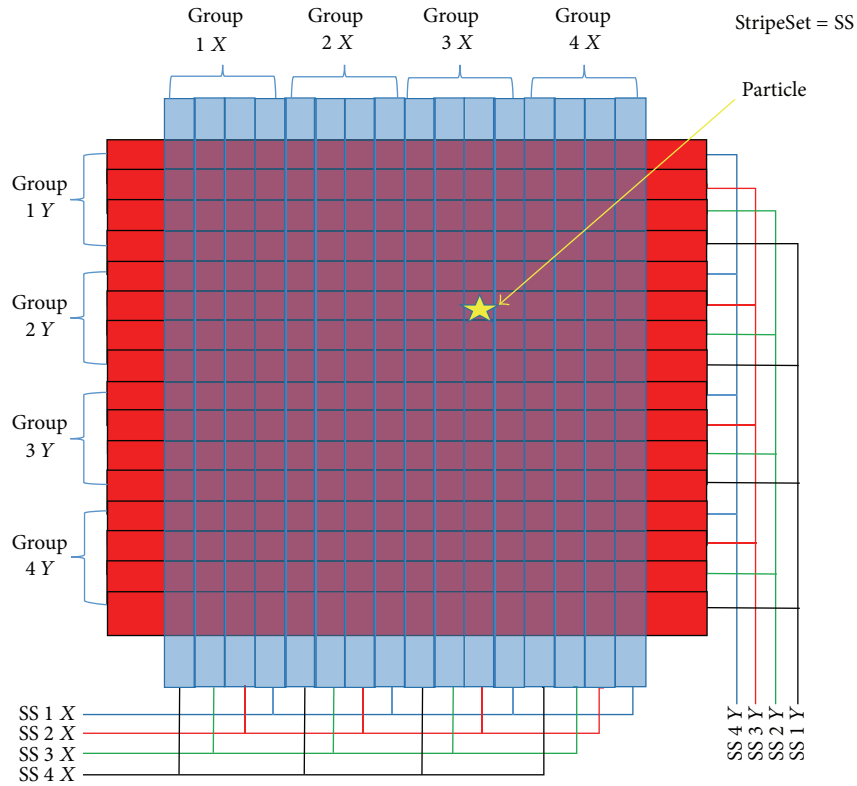
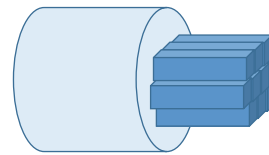
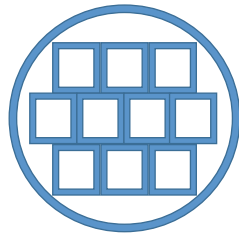


FIGURE 2: An example of the application of the channel reduction system.



Section view



Side view

(a)



(b)

FIGURE 3: (a) The optical coupling scheme and (b) photographs of the Sci-Fi and clear fiber prepared for coupling.

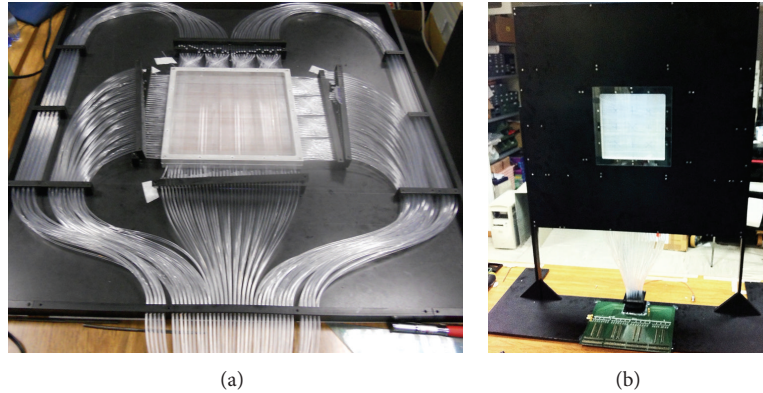


FIGURE 4: (a) The OFFSET tracker without the cover and (b) the complete OFFSET tracker.

output connectors fitting the data acquisition interface cable requirements. This module has 160 digital inputs/outputs and performs sampling up to 40 MHz and supports real-time analysis and DMA transfer to mass storage. Given this sampling frequency, the comparator output has been stretched up to 100 ns by the monostable in the front-end board in order to have at least three samples for each event. This choice limits the maximum rate to no more than 10 M particle/sec. Using a higher performance read-out module, it would be possible to attain up to 100 M particle/sec, which is the maximum rate allowed by the photomultiplier output signal characteristics. A real-time module, the PXIe-8102, is interfaced to the PXI-7813R through the PXI bus. A solid-state hard disk is used to store data. The PXIe-1062Q crate hosts the PXI-7813R, the real-time module, and the hard disk and has gigabit Ethernet communication to the acquisition PC. The identification of a pattern of at least four coincident high logic signals determines the trigger condition of the system. We have developed the firmware and the software for the OFFSET tracker data acquisition, analysis, display, and control, using the LabView software platform. National Instruments manufacture the electronic devices mentioned in this section.

**2.5. The Overall Detector.** Figure 4 shows two pictures of the final detector. In (a), without the cover, the sensitive  $20 \times 20 \text{ cm}^2$  area made of Sci-Fi and the routed clear fibers, which guide the scintillation light to the PSPM, are visible. In (b), with the cover, the front-end board is visible. The overall size of the detector, including the mechanical structure, is  $70 \times 100 \text{ cm}^2$ .

### 3. The Scintillating Fiber

A measurement campaign was performed on selected Sci-Fi for the OFFSET detector [10]. The fibers used are the  $500 \mu\text{m}$  size, square multi-cladding BCF-12 produced by SG [3].

**3.1. Light Generation and Transmission Properties in Sci-Fi.** The Sci-Fi have been characterized to measure the attenuation length of the light over the distance travelled from

the production point to the end of the fiber that is optically coupled to a photosensor. The manufacturer supplies a range of catalog specifications for all types of Sci-Fi with a diameter of one millimeter. It is not possible to extrapolate the specifications for different Sci-Fi diameters or cross-sections with a different shape. In particular, the submillimeter Sci-Fi have a dopant concentration higher than the concentration of the thicker fibers, which is responsible for a larger production of scintillation light. The higher dopant concentration is used to increase the light yield of the Sci-Fi but also influences their light attenuation performances. The manufacturer does not give the dopant concentration and, furthermore, this can slightly change from one stock of fibers to another. This is the main reason why the Sci-Fi needs a precise characterization before any application. The system used by SG to measure the attenuation length, for example, is to record the actual output of a bialkali photomultiplier, optically coupled to a Sci-Fi, in response to a  $^{90}\text{Sr}$   $\beta$  source placed at varying distances along the fiber, from one to three meters, to the photomultiplier.

The attenuation length of an optical fiber is defined as the distance at which the intensity of light travelling along the fiber is reduced to  $1/e$  of its initial intensity. From scientific literature [11, 12], the attenuation length function is the sum of two exponential terms, and, in this case, we can define two attenuation lengths acting in two distinct intervals of the distance travelled by the light along the fiber. Furthermore, the attenuation length is a function of the wavelength.

In this work we will consider only the integral attenuation length, convolution of the response of the Sci-Fi, and the quantum efficiency of the selected photomultiplier (PMT).

It should be noted that by definition the input light is generally considered as travelling along the fiber axis direction. In the case of scintillation light, this condition is not fulfilled because the light is produced isotropically inside the fiber and, therefore, only a fraction of the scintillation light is channeled into the fiber after a characteristic distance. Therefore, in our case the transmission properties for scintillation light and injected light are quite different.

**3.2. Attenuation Length.** In the first survey, the attenuation length function was extrapolated by projecting a pulsed laser beam of about 400 nm wavelength coaxially at one end of

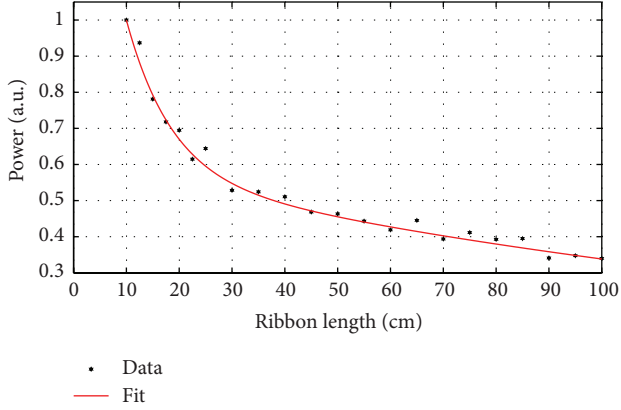


FIGURE 5: Plot of the data and the best fit relative to attenuation length measurement by coaxial laser injection.

TABLE 1: Extrapolated parameters: cut fiber.

Parameters	Values
$a$	1,417
$c$	0,6107
$\lambda_1$	8,52 cm
$\lambda_2$	173,55 cm

a ribbon of 8 Sci-Fi, using a bolometer to measure the amount of light collected at the other end. This measurement was made starting with a one-meter long Sci-Fi ribbon and repeated, shortening the length of the ribbon by cutting it each time, while trying to preserve the same conditions.

In this way, each measurement is the average of the results on the individual Sci-Fi, both in terms of the parameter dispersion of fibers and of the repeatability and uniformity of the ribbon-cutting and lapping procedure.

In dark conditions, the background level was recorded before turning on the laser beam to take each new measurement. A 10 MHz laser pulse frequency was chosen to fit the input dynamic range of the bolometer. The Sci-Fi ribbon was gradually shortened down to 10 cm. Figure 5 shows the power measured by the bolometer, normalized to its maximum value, for each fiber length.

Fitting the data by double exponential function in (2), we obtained the parameters reported in Table 1:

$$y(x) = ae^{-x/\lambda_1} + ce^{-x/\lambda_2} . \quad (2)$$

**3.3. Optical Coupling.** A preliminary step is to determine the asymmetry between the two channels, called Left and Right, mainly related to the different optical coupling or different quality of the ribbon-cutting procedure. It was carried out with an intense UV laser beam (wavelength 385 nm) illuminating the center of the ribbon and recording the average relationship between the charge measured by the two chains, PMTs and data acquisition electronics. The PMTs and the electronic chains were accurately characterized before the measurement. The two Thorn-EMI 9816B PMTs were set to about the same gain ( $\approx 2,4 \times 10^7$ ). After absorption, UV laser light produced scintillating light in the Sci-Fi.

The measurement was repeated by reversing only the channels of the acquisition system to eliminate offset and any differences in gain and sensitivity of the two channels. Figure 6 shows the charge spectra obtained with laser light for the Right (A) and the Left side (B).

Each of the figures shows the results obtained by reversing the A and B electronics and acquisition channels. In effect, the results, which take into account the differences of the various parameters, are essentially the same, showing a deviation of less than 2%. The laser light is injected perpendicularly into the center of the ribbon and, therefore, the light is attenuated along the fibers by the same amount in each direction. It follows that the relationship between the centroids of the spectra of the Left and Right PMTs is the ratio between the different attenuations due to the optical coupling between the PMT and fiber ribbon, taking into account the differences between the PMT and electronic channels.

**3.4. Measurement with UV Light.** A widely used method for the characterization of the Sci-Fi is to move a particle source along the fiber and to measure the light at its ends.

We designed a different measuring apparatus in which the scintillation was produced by incident particles perpendicular to the Sci-Fi ribbon, thus ensuring a constant amount of isotropic light, regardless of the entry point of the particle in the scintillator. We used a UV laser beam controlled by a pulse generator which, passing through a collimator, hits a ribbon consisting of four 500  $\mu\text{m}$  square Sci-Fi in a very small area, that is, only 3 mm. Figure 7 shows the experimental setup, schematic view, and picture. Two PMTs are optically coupled to the opposite edges of a Sci-Fi ribbon. The light source is mounted on a slide.

The block diagram of the data acquisition system employed for the measurement is shown in Figure 8. The electronic chains for the two PMTs are the same as for cosmic ray measurement.

The acquisition of the input signal is controlled by a trigger signal whose duration is the time window of measurement (GATE). This signal, leaving the connections unit, is present only if the pulses from the PMTs coincide with the sync-out signal of the laser. The combination of attenuator and amplifier modules at the output of the PMTs is used to fit their signal charge with the input dynamic range of the two QDCs.

**3.5. Comparison of the Results.** These two measurements are not actually comparable for reasons relating to the mechanism of light production. In the first case, light is injected at one end of the fiber ribbon and read at the opposite end, after the cut and lap procedure. In the second case the scintillation light is produced by a UV laser beam positioned perpendicularly with respect to the fiber with almost constant intensity. The different mechanisms of production and propagation of light in the two cases explain the different results regarding the attenuation length measurement. Figure 9 shows a plot of the two derived attenuation length functions.

The fit parameters for the two measurements are summarized in Table 2. The parameters refer to (2).

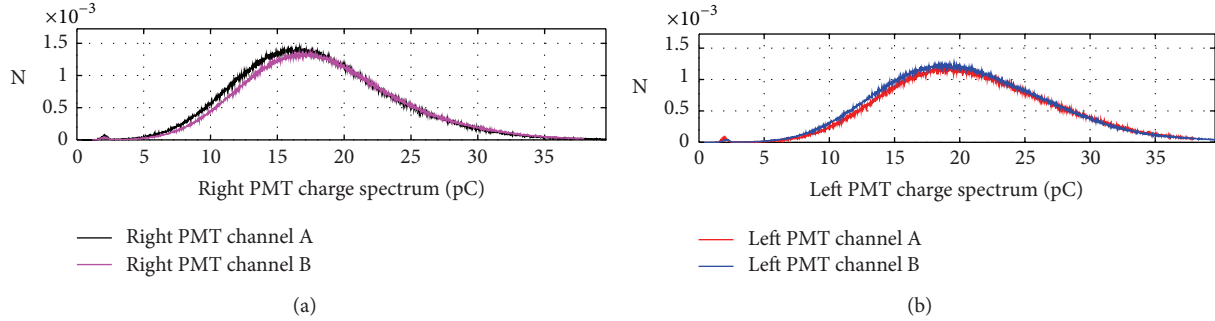


FIGURE 6: Charge spectra for the Right PMT (a) and for the Left PMT (b) obtained by injecting the UV laser into the center of the fiber ribbon and reversing the electronic chains.

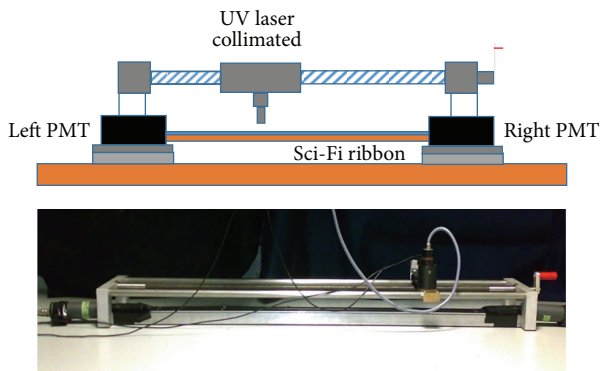


FIGURE 7: Schematic view and picture of the experimental setup.

TABLE 2: Summary of the fit parameters.

Technique	Parameters	Values
Cut and lap	$a$	1,346
	$c$	0,58
	$\lambda_1$	8,5 cm
	$\lambda_2$	1,74 m
UV laser	$a$	1
	$c$	0,65
	$\lambda_1$	8,52 cm
	$\lambda_2$	1,05 m

**3.6. GEANT4 Simulations on the Fibers Response to Proton Beams.** The simulation software was adapted to meet the case of protons that pass through the fiber ribbon perpendicularly.

This result was provided thanks to GEANT4 simulations. Note that in the case of the proton beam the simulated trace length is not very different and it plays an important role in the efficiency of the scintillating fiber. The spectrum of energy deposited on fibers by 62 MeV protons is shown in Figure 10. Notice that the average energy released in these conditions by the particles is  $\sim 546$  keV.

A similar simulation was carried out with 250 MeV protons considering the specific requirements for the detector. In this case, the average energy released, according to the simulation, is 408 keV and therefore lower than for the 62 MeV protons. Given that consideration, the paper continues assuming the context of the 250 MeV protons as the condition in which the scintillation light is lower.

Using fiber ribbons of the type previously considered to build the detector, not all of the tape forms part of the sensitive area. Indeed, a part of the tape is used for optical coupling. The simulation takes it into account generating protons only on the sensitive area, as shown in blue in Figure 11. In any case, when the attenuation of the scintillation light from the scintillating fibers is calculated, the entire length of the tape must be considered, including both the yellow and the blue areas as shown in Figure 11.

The expected output spectra from the two photomultipliers are shown in Figure 12. As can be observed, there are no highlighted single or double photoelectron peaks.

The distribution of photoelectrons detected by the two photomultipliers for the protons is plotted in Figure 13, which shows that the responses of the two photomultipliers cannot be superimposed. The peak of the distribution of the photomultiplier called PMT<sub>1</sub> has moved further to the left, indicating that less photoelectrons are detected. This effect is mainly due to the different distances at which the sensitive photomultipliers have been placed to simulate the needs of real techniques, as shown in Figure 15. The small differences between the two spectra are due to the different gains and optical couplings between the two channels.

Figure 14 shows the average number of photoelectrons detected by the two PMTs as a function of the proton impact position on the fiber measured, starting from PMT<sub>1</sub>. Figure 14 also shows the number of simulated PMT signals in coincidence for a given threshold and an average detection efficiency of 99.9%.

The results are, therefore, that, in the case of 250 MeV protons, the detection efficiency increases just for the events relating to the sensitive area and the central ribbon. As in the previous case regarding muons, events related to the extreme zones of the belt are more likely to produce noncoincidence between the two photomultipliers and then to be lost in the acquisition phase. In these conditions, however, the average efficiency occurs almost constantly throughout the ribbon.

If we consider a detector consisting of two superimposed planes of fibers oriented perpendicularly to each other, it can be deduced that the detection efficiency is the total square of the one previously mentioned. Since this is 99.9%, this suggests that the efficiency of the detector remains completely unchanged.

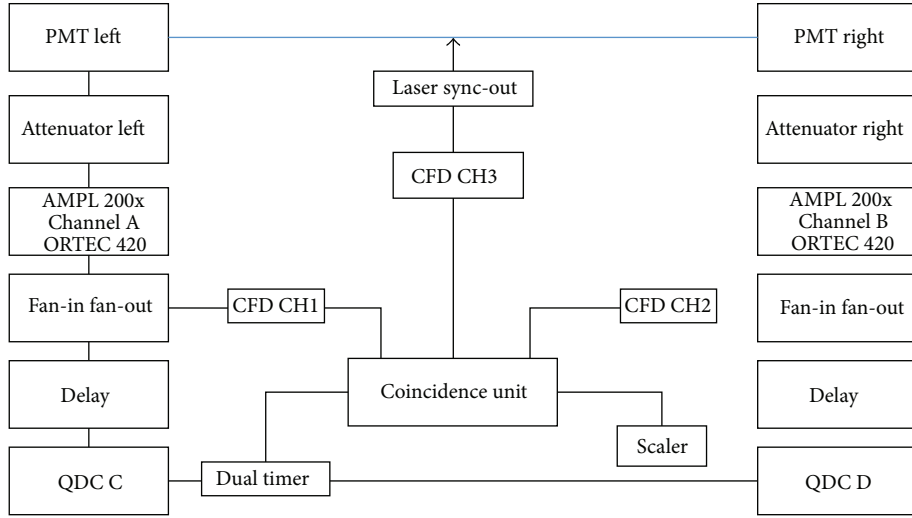


FIGURE 8: Block diagram of the data acquisition system.

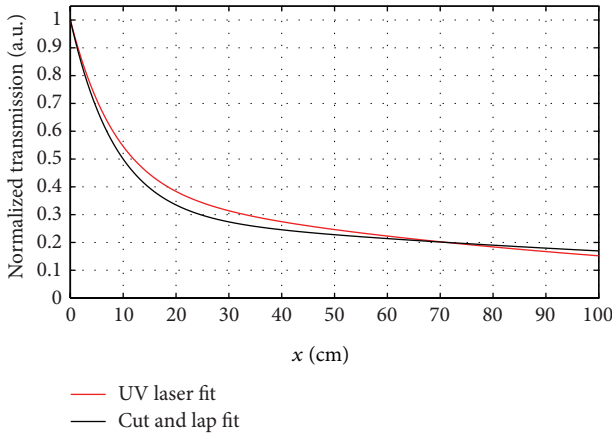


FIGURE 9: Plot of the two normalized attenuation length functions. In blue, the attenuation length for the cut and lap quality control, with coaxial light injection. In red, the attenuation length function obtained by UV laser.

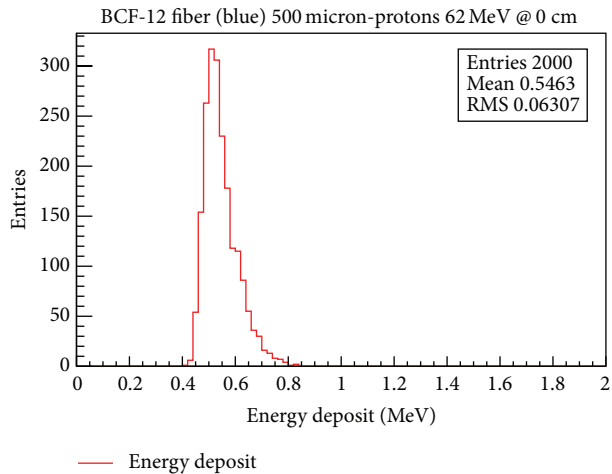


FIGURE 10: GEANT4 simulation of protons, which pass through the fiber ribbon perpendicularly. Spectrum of energy released by 62 MeV protons on the BCF-12 fibers.

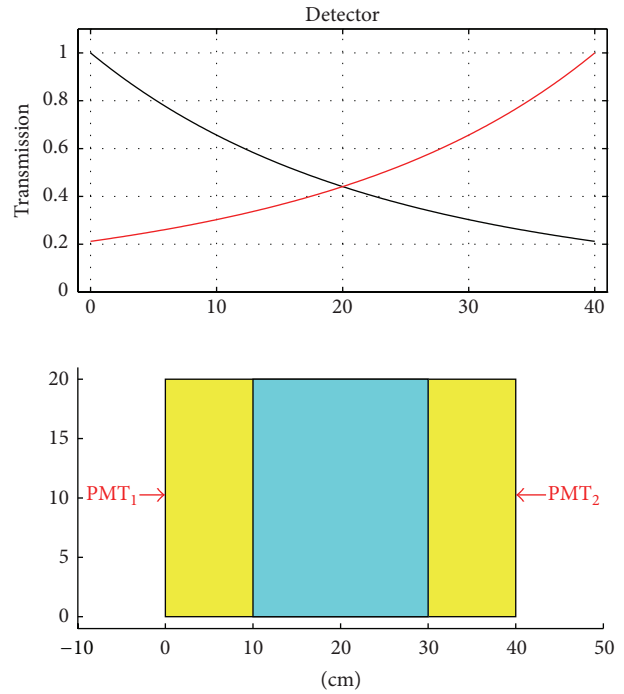


FIGURE 11: Transmission and sensitive area in the detector  $20 \times 20 \text{ cm}^2$ .

It is evident that it is possible to design a detector with the services requested in advance/to advance specifications. It should however be noted that, given the fact that the OFFSET detector is subject to loss of scintillation light due to the optical couplings, multianode super bialkali photomultipliers with high quantum efficiency could be employed to ensure good detection efficiency margins. A simulation using a photomultiplier with a QE equal to 35% is shown in Figure 15.

It should be remembered that these results were obtained for 250 MeV protons. This is an unfavorable condition with respect to the 62 MeV protons.

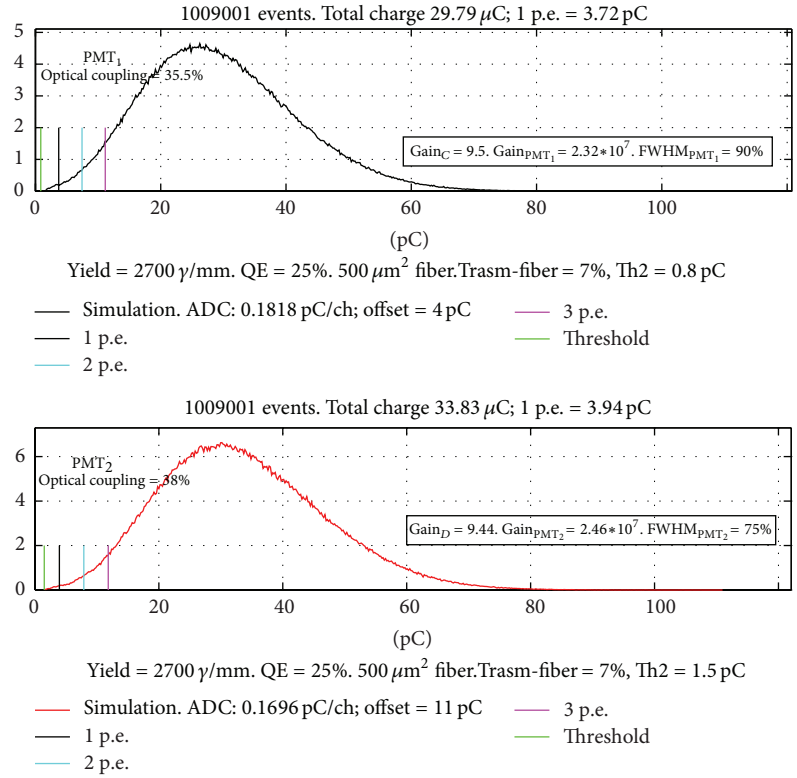


FIGURE 12: Spectra simulated of the output to the two photomultipliers.

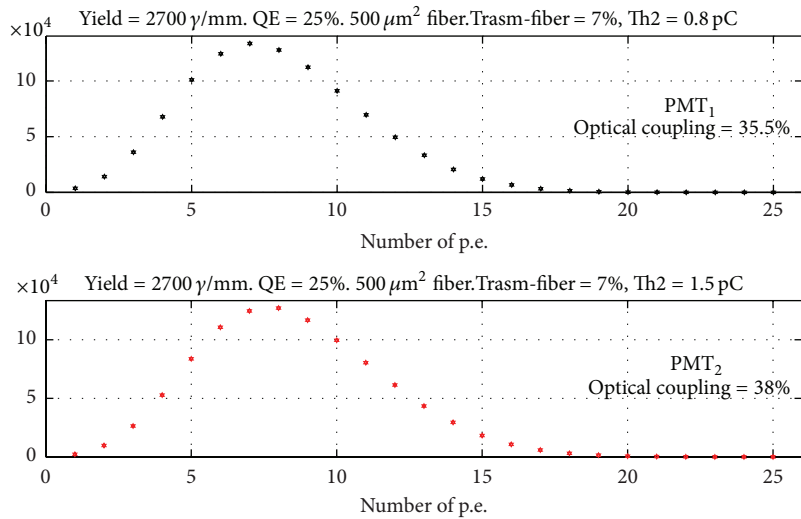


FIGURE 13: Spectra of the expected output from the two photomultipliers in a number of photoelectrons.

In conclusion, the different production mechanisms of the scintillation light determine different integral attenuation length functions. Two exponential law components may be distinguished: one short and one long.

#### 4. OFFSET Tests

The design of the OFFSET tracker started with simulation studies in order to evaluate the detector architecture on

the basis of its response to different stimuli: cosmic rays,  $\beta$  sources, and proton beams at different energies. Nevertheless, the GEANT4 simulations [13] of submillimeter Sci-Fi were not decisive, due to a lack of sufficient factory information. However, the scientific literature [12, 14] provides some essential reference points for the design of the detector. The best way is to directly measure the selected Sci-Fi coupled to the selected photo-sensor in order to find, for example, the maximum size limits that the detector can reach. The OFFSET tracker is well below these limits. The OFFSET



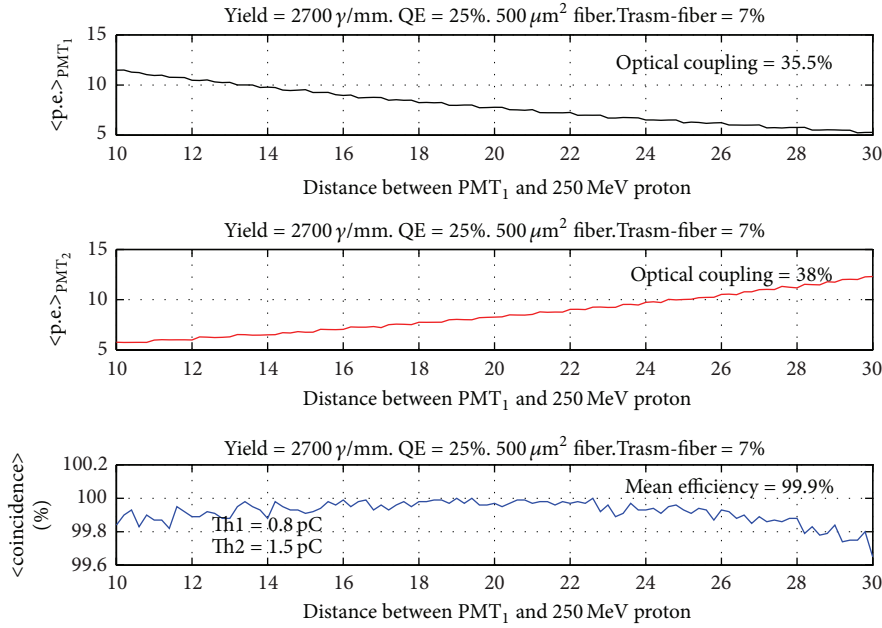


FIGURE 14: Photoelectrons produced as a function of the impact position for the two PMTs and detection efficiency.

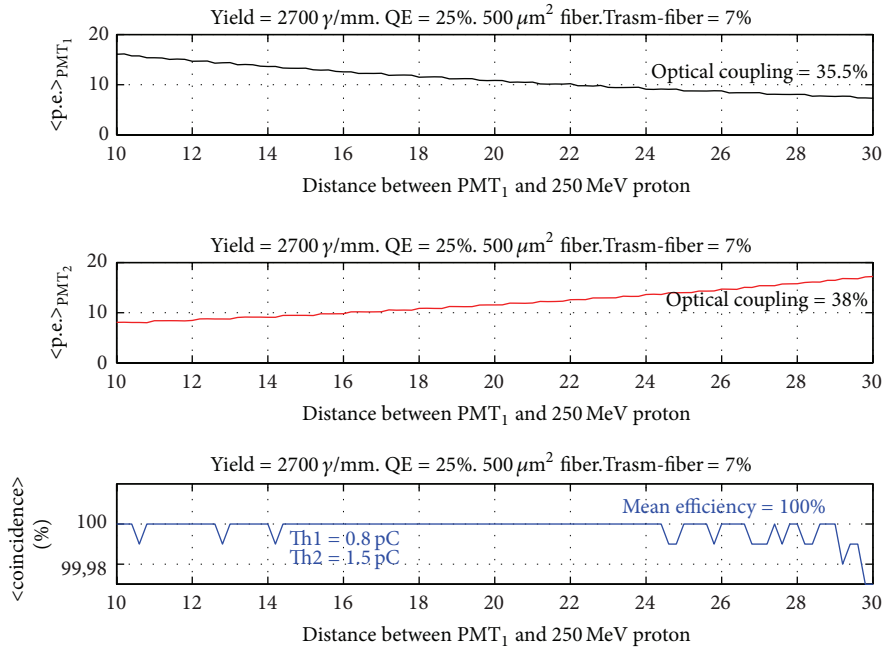


FIGURE 15: Simulation similar to Figure 14 adopting photomultipliers with a QE of 35%.

detector was tested using  $\beta$  sources, cosmic rays, and proton beams.

4.1. Tests Using  $\beta$  Sources and Cosmic Rays. We have preliminarily tested the OFFSET detector using two different sources:  $\beta$  sources and cosmic rays. The use of  $\beta$  sources is very useful because it allows an image to be produced in the worst possible conditions, that is, with low linear energy transfer particles, and also to bench-test the detector without the limitations of an accelerator room. Figure 16 shows a

real-time image of a  $90\text{Sr}$   $\beta$  source with a 2 cm diameter. Some lines are clearly missing. These lines correspond to the tenth fiber of each Sci-Fi group and indicate a worse optical coupling than in the other groups, due to the Sci-Fi routing procedure. An important test is the detection of cosmic rays because they are minimum ionizing particles (MIP) and they represent a diffused source of low energy transfer particles. It should be noted that the 250 MeV proton beam used for medical imaging is equivalent to about 2 MIP. The image provides additional information: first, the level of uniformity

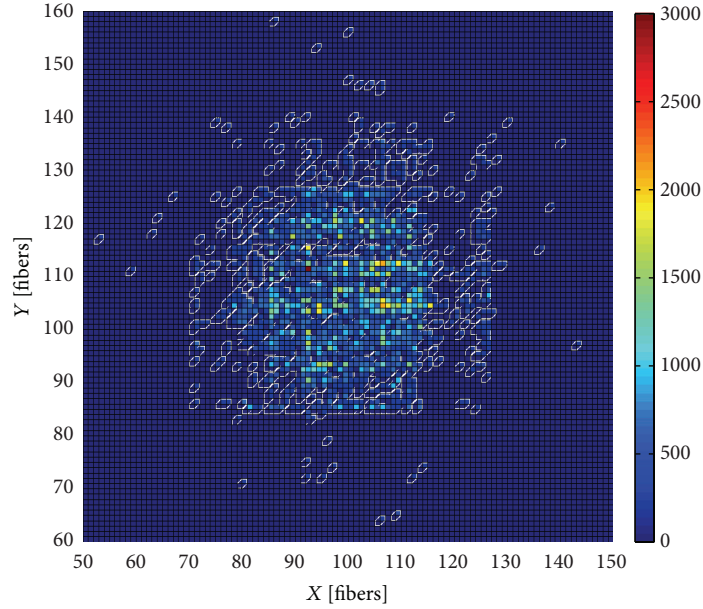


FIGURE 16: Real-time image of a 3 KBq  $^{90}\text{Sr}$   $\beta$  source acquired by the OFFSET tracker. Axis units are in fibers number. The exposure time, needed to reach the three millions of events prefixed for the image, is of about 30 minutes.

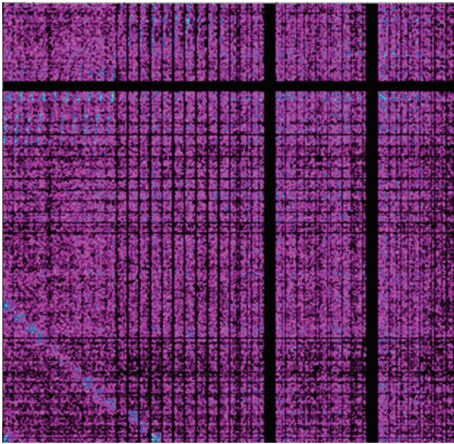


FIGURE 17: Image, due to the cosmic rays, acquired by the OFFSET tracker.

in the detector response and second, the level of efficiency of the detector. Figure 17 shows the image of the cosmic rays acquired in 47 hours, relative to the entire active area of the detector. Three groups of Sci-Fi, ten Sci-Fi each, are absent in the image. This is due to the failure of their front-end channels. Some vertical and horizontal lines are missing for the same reason as given in the case of the test using  $\beta$  sources.

**4.2. Test with 62 MeV Protons.** The prototype of the tracker plane has also been tested with a 62 MeV proton beam in the CATANA [15] facility at the LNS.

Before measuring, the CATANA staff performed a beam profile characterization along the X and Y directions employing calibrated diodes. The result is shown in Figure 18. In order to perform a precise calibration of the detector, a

gafchromic EBT [16] film was fixed to the portion of the sensitive area crossed by the proton beam. Using the beam profile characterization, we have calibrated the gafchromic film. Figure 19 shows a sketch and a picture of the experimental setup.

The comparison between the standard beam profile and the measurements with OFFSET allowed the imaging performances of the tracker to be extracted. A long run, up to about 1.6 Gy, was performed using all beam spots and then an eye-shaped collimator. The calibrated gafchromic EBT film was digitized with a scanner and the final dose distribution was used to calibrate the region of the sensitive area of the tracker intersected by the beam. The calibration was performed by summing, for each pixel, all the images acquired, based on the reasonable assumption that any nonuniformity in the pixel response in the sensitive area was time invariant. The same calibration matrix produced using the beam spot was used to correct the eye-shaped image and the results are shown in Figure 20. In this image, it is possible to see where the dashed circle representing the calibration area of interest ends and how it influences the eye-shaped collimator image.

Another long run, up to about 1.2 Gy, was performed using a 1.5 cm diameter-hole calibrated collimator. During this run, an image of the beam was recorded in real time every minute. In this case, there are no missing fiber groups, such as in the previous acquisition (Figures 16, 17, and 20) thanks to the repair of the front-end board. The lack of uniformity is mainly due to the different optical couplings between the fibers and the PSPM and the non-uniformity of the PSPM photo cathode gain.

Figure 21 shows the results of the test. Starting from the gafchromic EBT film image and the raw sum of all the images acquired with the hole collimator, a calibration matrix was obtained. Once calculated, the calibration matrix was then applied to each image acquired.

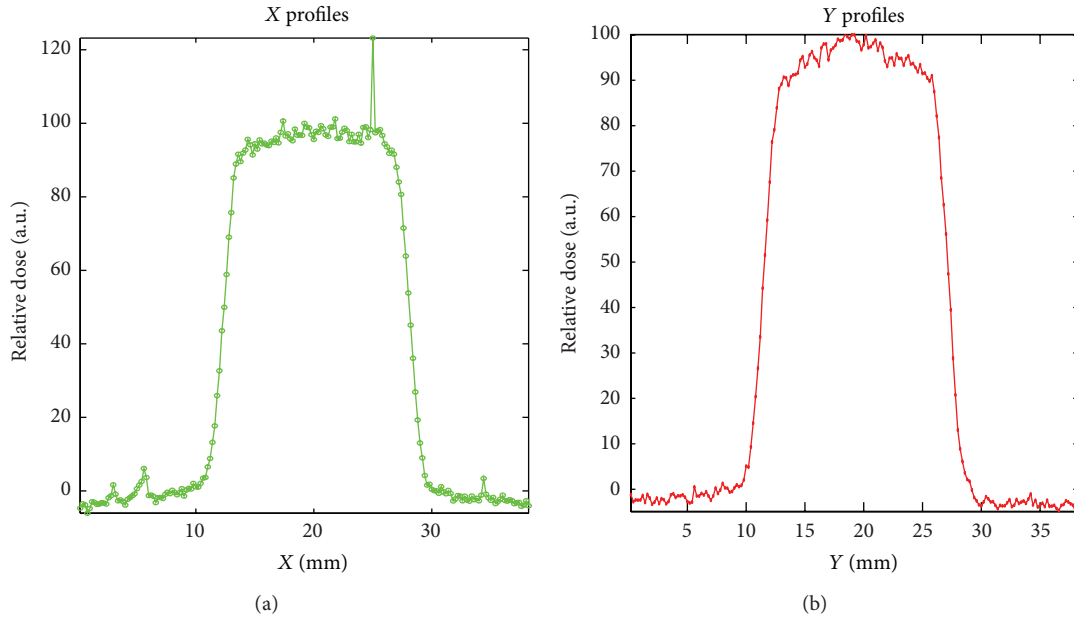


FIGURE 18: Beam profile characterization acquired with calibrated diodes.

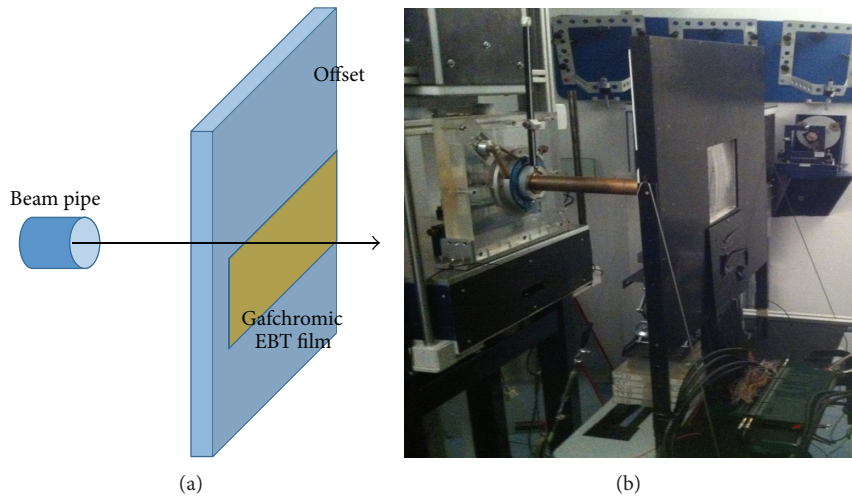


FIGURE 19: Drawing (a) and picture (b) of the experimental setup inside the CATANA hadrontherapy facility.

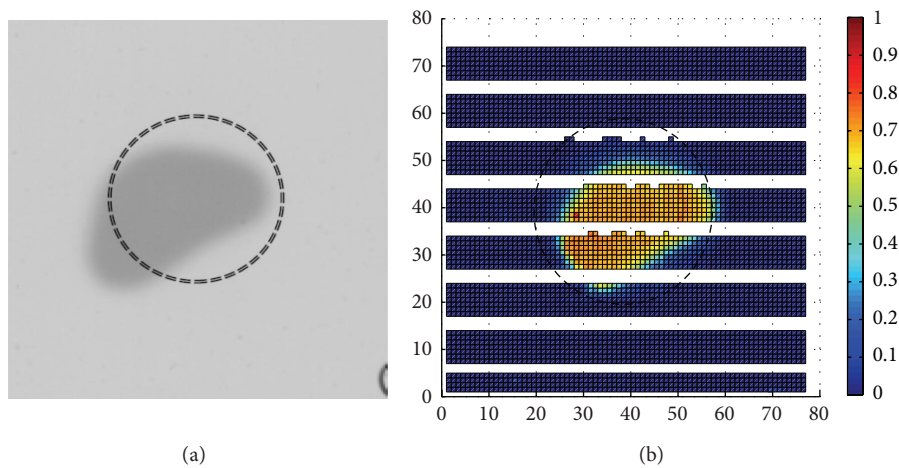


FIGURE 20: (a) The gafchromic EBT film image and (b) the eye-shaped image, calibrated. Axes are in fibers number (fiber size  $500 \mu\text{m}$ ).

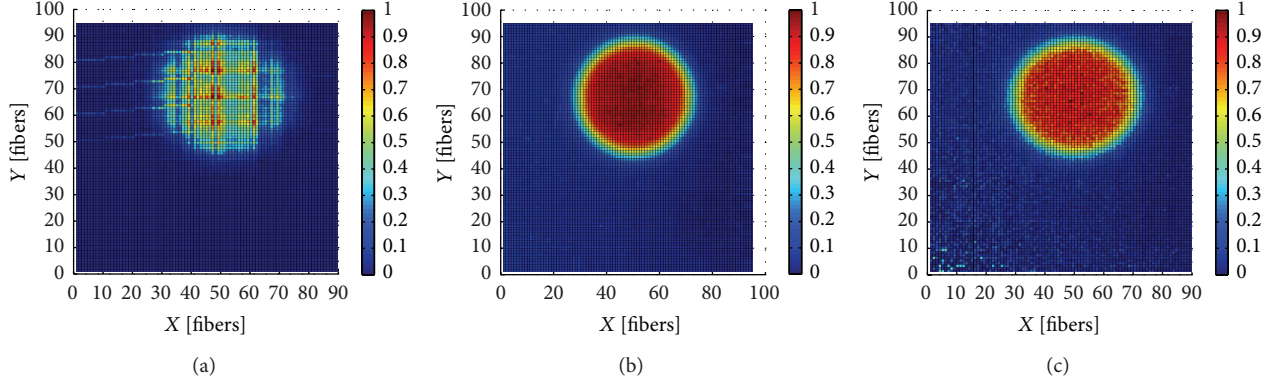


FIGURE 21: (a) The gafchromic EBT film image, (b) the raw sum of all the images with OFFSET, and (c) the corresponding image, calibrated. Axes are in fiber units ( $500 \mu\text{m}$ ).

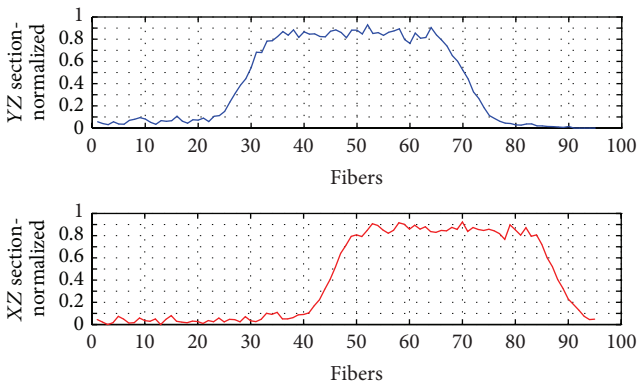


FIGURE 22: Beam profiles monitored during time by the OFFSET tracker.

After calibration, each one-minute frame was analyzed in order to perform a beam profile characterization, monitoring the beam profile during time. Figure 22 shows this result.

**4.3. Efficiency.** In order to determine the detection efficiency of the prototype, a constant fraction discriminator measured the rate  $r_{\text{CFD}}$  (about 70 kparticle/sec) of the particles that crossed the sensitive area of the detector, mainly due to the light produced in the scintillating fibers. The measurement was made using the dynode signal of the PSPM connected to the input of a SensL CFD [17]. The PSPM dark rate of about 100 Hz is negligible. The  $r_{\text{CFD}}$  was compared with the rate measured with a plastic scintillator read by a bi-alkali photomultiplier, placed after the OFFSET tracker downstream of the beam. Correcting the dead area of the detector (mainly due to the cladding), the two measured rates were about the same (the ratio of the rates is about 0.9 and the dead area due to the cladding about 10%). Therefore,  $r_{\text{CFD}}$  was taken as the reference value for the detector efficiency calculation.

Then we measured the rate  $r_{\text{Tt}}$  of tracks recorded by the detector read-out using the trigger condition described in Section 2.4. Some events are missing due to the lack of some vertical and horizontal lines. We have estimated the rate  $r_{\text{Te}}$  of tracks in these lines to be the average of the neighbour pixels. In this way, the total rate  $r_{\text{Tt}}$  of tracks can be evaluated as the

sum  $r_{\text{Tt}} + r_{\text{Te}}$ . Then the detection efficiency of the sensitive area  $\eta_D$  is expressed by the ratio  $r_{\text{Tt}}/r_{\text{CFD}}$ , which results to be 80.5%.

As already mentioned the sensitive area of the detector is reduced by the multicladding of the fiber, which is naturally not taken into account by  $r_{\text{CFD}}$ . In an  $X$ - $Y$  square detector with length  $L$  that uses square fibers of thickness  $r_f$  with a multicladding that is  $t_c$  thick, the active area can be calculated as

$$S_a = \left(1 - 2 \frac{t_c}{t_f}\right)^2 L^2. \quad (3)$$

Then the geometric efficiency is

$$\eta_G = \left(1 - 2 \frac{t_c}{t_f}\right)^2. \quad (4)$$

The employed fibers have  $t_c/t_f = 0.06$ , and then  $\eta_G$  can be evaluated as about 77%. Then the total detection efficiency  $\eta_T$  of the OFFSET tracker is

$$\eta_T = \eta_D \times \eta_G. \quad (5)$$

With all the detector channels working, we would expect  $0.8 \times 0.77$  that is 62% efficiency.

## 5. Conclusion and Outlook

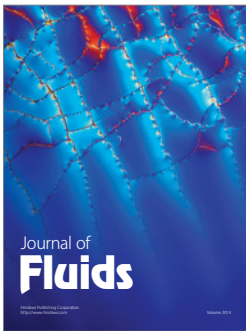
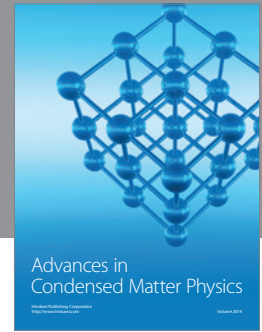
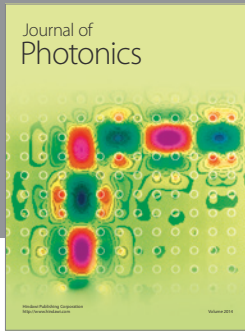
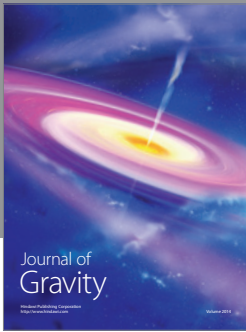
The paper presents a characterization technique for selected scintillating fibers to extract the main design specifications. The first prototype of the OFFSET tracker was designed and tested with  $\beta$  sources, cosmic rays, and a proton beam. The system is easily and reproducibly assembled. In addition, it has the great advantage of a system to reduce the read-out channels applied to a large area and high spatial resolution detector, employing submillimeter Sci-Fi. A complete characterization was carried out and the results were presented. A new version of the detector is now under construction in order to reduce its overall size, improve its imaging performances, and extend the sensitive area to  $30 \times 30 \text{ cm}^2$ . The obtained results demonstrate the validity of the designed read-out technique, which has been patented by the INFN [18].

## Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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