

Methane production by mechanochemical processing of MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> as sources of H<sub>2</sub> and CO<sub>2</sub> at room temperature

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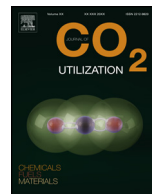


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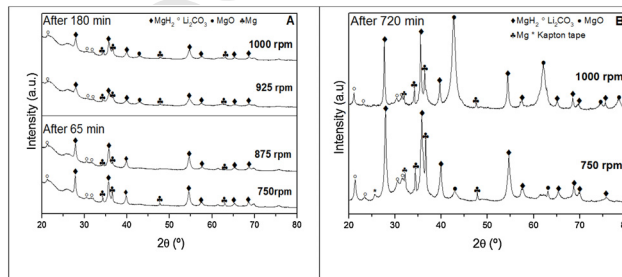
Graphical abstract



### Methane production by mechanochemical processing of MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> as sources of H<sub>2</sub> and CO<sub>2</sub> at room temperature

María L. Grasso\*, Luisa Fernández Albanesi, Sebastiano Garroni, Gabriele Mulas, Fabiana C. Gennari

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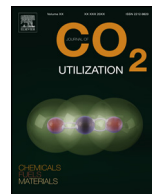


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### Highlights

#### **Methane production by mechanochemical processing of MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> as sources of H<sub>2</sub> and CO<sub>2</sub> at room temperature**

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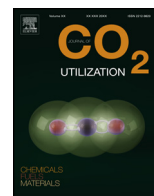
María L. Grasso\*, Luisa Fernández Albanesi, Sebastiano Garroni, Gabriele Mulas, Fabiana C. Gennari

- CH<sub>4</sub>/H<sub>2</sub> fuel mixture is obtained by mechanical milling of MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> at room temperature.
- Mechanochemical process occurs without catalyst and with high selectivity to methane.
- Analyses of the gas-product evolution evidences the absence of CO<sub>2</sub> or CO during milling.
- Methane generation is kinetically restricted by the high stability of Li<sub>2</sub>CO<sub>3</sub>.
- Solid products are reused as CO<sub>2</sub> absorbers for the exhaust gases treatment of power plants.

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# Methane production by mechanochemical processing of MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> as sources of H<sub>2</sub> and CO<sub>2</sub> at room temperature

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## ABSTRACT

The reutilization of CO<sub>2</sub> to produce valuable chemical fuels is an attractive approach to reduce the greenhouse effect and global warming. In this work, the room temperature production of CH<sub>4</sub>/H<sub>2</sub> fuel mixtures via mechanochemical activation of Li<sub>2</sub>CO<sub>3</sub>-MgH<sub>2</sub> system was explored. The CH<sub>4</sub>/H<sub>2</sub> fuel mixtures were obtained by a free-catalyst reaction, with high selectivity and using Li<sub>2</sub>CO<sub>3</sub> and MgH<sub>2</sub> as solid portable sources of CO<sub>2</sub> and H<sub>2</sub>, respectively. The effect of processing parameters on both the evolution of the solid phases and the production of CH<sub>4</sub>/H<sub>2</sub> fuel mixtures was studied using X-ray diffraction, spectroscopic techniques, electron scanning microscopy and gas chromatography. Thermodynamic calculations predict the complete CO<sub>2</sub> reduction to CH<sub>4</sub>, with simultaneous formation of MgO and Li<sub>2</sub>O. Experimental evidence supports the progressive formation of MgO and the appearance of Li<sub>2</sub>O. The presence of H<sub>2</sub> simultaneously with CH<sub>4</sub> in the gas phase was due to kinetic restrictions. Based on experimental results and equilibrium composition calculations, the reaction mechanism was proposed. The kinetic analysis reveals that the rate limiting CH<sub>4</sub> production is the nucleation of MgO/Li<sub>2</sub>O in the surroundings of Li<sub>2</sub>CO<sub>3</sub>, while the H<sub>2</sub> release is controlled by the reaction interface between MgH<sub>2</sub>/Mg or MgH<sub>2</sub>/MgO.

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## 1. Introduction

Carbon dioxide gas (CO<sub>2</sub>) is considered one of the main contributors to global warming and climate change because of its role in the greenhouse effect. Human activities, such as combustion of fossil materials (coal, oil, natural gas), industrial processes, changes in land use and deforestation, are considered to be the main responsible for the growing CO<sub>2</sub> atmospheric concentration, from 280 ppm in the pre-industrial era to 415 ppm in 2019 [1], with an increase of 0.8 °C in global planet temperature. Intergovernmental Panel on Climate Change (IPCC) has estimated that by the end of the century, CO<sub>2</sub> concentration would reach 700 ppm and the average temperature would increase up to 5 °C, with devastating and irreversible climate changes [2]. For these reasons,

a current and urgent challenge is to find a sustainable way to reduce CO<sub>2</sub> concentration in the atmosphere. Unfortunately, the continuous increase in energy demand due to a growing population and life-style quality implies more CO<sub>2</sub> atmospheric emissions [3].

Carbon dioxide capture and utilization (CCU) is a very promising strategy to mitigate CO<sub>2</sub> emissions, having at the same time a benefit related to the production of value-added products. Here, CO<sub>2</sub> acts as a carbon source to synthesize products such as alcohols, polymers and synthetic fuels. Also, there are direct applications of the captured CO<sub>2</sub>: in carbonated drinks, as dry-ice, in fire extinguishers or in algae farms for photosynthesis [3,4]. Among synthetic fuels to be produced from CO<sub>2</sub>, methane is the hydrocarbon with the highest hydrogen to carbon ratio. Its gravimetric heat is greater (55.5 MJ/kg) than butane (49.5 MJ/kg), diesel (44.8 MJ/kg) and methanol (22.7 MJ/kg) [5]. In addition, CH<sub>4</sub> is compatible with our current storage and distribution network. Based on its good properties, methane is considered an attractive and alternative fuel. Interestingly, the addition of H<sub>2</sub> to CH<sub>4</sub> produces a fuel-gas mixture with improved properties for its

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use in stationary applications like heaters, boilers and turbines or in mobile applications like internal combustion engines and gas turbines [6,7]. In fact, the wide ignition limits and high flame speed of hydrogen have a positive impact on the combustion, improving the energy density of natural gas on the operation conditions. In addition, mixtures of H<sub>2</sub> with CH<sub>4</sub> allow a substantial reduction of the CO<sub>2</sub> emissions. These hydrogen-enriched mixtures (up to 20 %) can be distributed by the mid-pressure natural gas network or stored under pressure using conventional methane storage technologies without substantial technical modifications [8].

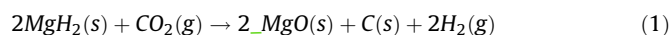
In the search for alternative methods of CO<sub>2</sub> hydrogenation, our working group has recently reported the use of Mg-Fe and Mg-Ni complex hydrides with a dual function: as promoters of the CO<sub>2</sub> conversion and as hydrogen sources [9,10]. CO<sub>2</sub> methanation was promoted by the presence of Fe, Ni and/or Mg-Ni alloys obtained during decomposition of the Mg<sub>2</sub>FeH<sub>6</sub> and Mg<sub>2</sub>NiH<sub>4</sub> hydrides, while its conversion depended on the nature of the hydride, the experimental conditions and the H<sub>2</sub>:CO<sub>2</sub> molar ratio [9]. The global mechanism for both hydrides includes the reversed water-gas shift reaction followed by CO methanation in presence of steam. However, in the case of Mg<sub>2</sub>NiH<sub>4</sub>, the direct reduction of CO<sub>2</sub> by MgH<sub>2</sub>/Mg<sub>2</sub>NiH<sub>x</sub> hydrides takes an important role in the whole process. Refinement of the Mg<sub>2</sub>NiH<sub>4</sub> microstructure to the nanometric scale modifies the CO<sub>2</sub> methanation mechanism [10] and it proceeds by adsorption of C and direct solid gasification toward CH<sub>4</sub> formation.

In this context, the development of simple methods for CO<sub>2</sub> conversion into valuable chemicals or energy carriers under soft conditions (mild pressure and temperature) is a topic of interest in the scientific community. In this respect, the mechanochemical synthesis is considered a manufacturing technology that is simple, efficient, cheap, scalable, low-waste, and solvent-free for the production of chemicals at room temperature [11,12].

Mechanochemical activation of different solids was applied to promote CO<sub>x</sub> storage and/or its conversion via different solid-gas reactions [13–17]. Mulas et al. studied the mechanochemical hydrogenation of CO over FeCo and Mg<sub>2</sub>Ni-based catalysts [13]. Chemical transformations were promoted by mechanical treatment at the interface of solid-gas systems at mild conditions. The CO<sub>2</sub> conversion to CH<sub>4</sub> obtained via FeCo catalysts at room temperature and atmospheric pressure is similar to the corresponding one occurring in thermally activated conditions, which requires high temperature and pressure. In addition, a recent investigation reported the production of CH<sub>4</sub> and light hydrocarbons by milling of the olivine (a magnesium silicate mineral) and water under CO<sub>2</sub> atmosphere [14]. Energetic ball milling promotes the olivine-water activation, releasing H<sub>2</sub> and allowing the hydrogenation of CO<sub>2</sub> by the in situ formation of magnetite-based catalysts [15]. The mechanism of the whole process is complex, and competitive processes such as the precipitation of carbonate phases were also detected as dependent on the CO<sub>2</sub>/H<sub>2</sub>O ratio. These investigations exhibit the potential of mechanochemical processing to promote gas-solid reactions in the presence of catalysts and under mild conditions.

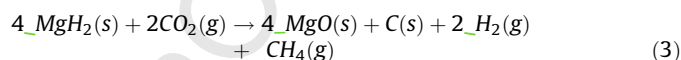
In this line, two recent investigations reported the mechanochemical conversion of CO<sub>2</sub> to produce CH<sub>4</sub>-H<sub>2</sub> mixtures using light metal hydrides (LiH, NaH, MgH<sub>2</sub> and CaH<sub>2</sub>) as hydrogen source at room temperature and without any catalyst [16,17]. Dong et al. were the first to produce CO<sub>x</sub>-free mixtures of CH<sub>4</sub>-H<sub>2</sub> through a solid-gas mechanochemical reaction. The yield of CH<sub>4</sub> was dependent on the nature of the light metal hydride, rate and duration of ball milling, and CO<sub>2</sub> pressure. The selectivity also depends on these parameters, detecting CO formation at high CO<sub>2</sub>:H<sub>2</sub> ratios. Experimental results indicated that the mechanism of

CO<sub>2</sub> reduction using MgH<sub>2</sub> (or LiH) involves the production of amorphous carbon followed by a hydrogenation step:

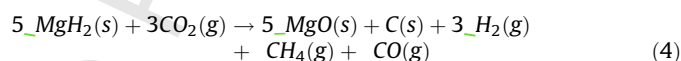


The reaction between carbon and H<sub>2</sub> produced *in situ* during mechanochemical processing is responsible for the CH<sub>4</sub> formation.

Using a similar strategy, Pu et al. investigated the effect of different H<sub>2</sub>:CO<sub>2</sub> ratios on the conversion efficiency of CO<sub>2</sub> to CH<sub>4</sub> by mechanochemical reduction with light metal hydrides. According to the X-ray diffraction (XRD), Fourier transform infrared spectroscopy (FTIR) and X-ray photoelectron spectroscopy (XPS) data, the following reaction mechanism was proposed for H<sub>2</sub>:CO<sub>2</sub> molar ratio lower than 2:1:



As the concentration of CO<sub>2</sub> was increased, CO formation was observed. For H<sub>2</sub>:CO<sub>2</sub> ratio of 7:5, the solid products formed were MgO, MgCO<sub>3</sub> and C, and the global reaction can be described by:



These investigations demonstrated that the mechanism of CO<sub>2</sub> reduction by light metal hydrides depends on several factors. In general, LiH and MgH<sub>2</sub> hydrides, contrary to NaH, favor the reduction of CO<sub>2</sub> to CH<sub>4</sub>.

Recently, Dong et al. studied the interaction between metal hydrides and alkaline carbonates as sources of H<sub>2</sub> and CO<sub>2</sub>, respectively [18]. This study consisted in following the reactivity of MH-M<sub>2</sub>CO<sub>3</sub> systems (where M = Mg or Ca) during mechanical milling at room temperature under catalyst-free conditions. The authors reported a highly selective method to CO<sub>2</sub> conversion and to synthesize CO<sub>x</sub> free H<sub>2</sub>/CH<sub>4</sub> blends. Different parameters such as prolonged milling times of 48 h, high ball milling rates (450–550 rpm), and high H<sub>2</sub>:CO<sub>2</sub> ratios promote the formation of CH<sub>4</sub> as the only hydrocarbon product. The analysis of the gas and solid products show that the methanation reaction occurs between the H<sub>2</sub> released from the hydride and amorphous carbon produced by carbonate reduction. This reaction mechanism is similar to the one proposed by the same research group during mechanochemical reduction of CO<sub>2</sub> gas using light metal hydrides [17].

On the basis of previous knowledge, the replacement of gaseous CO<sub>2</sub> and H<sub>2</sub> by solid alkaline carbonates and hydrides to carry out the CO<sub>2</sub> conversion process, presents some advantages. From the point of view of materials manipulation, inorganic carbonates are inexpensive, abundant, and easy to handle under air atmosphere. As an extra advantage, some carbonates are the main product obtained after CO<sub>2</sub> capture by absorbents like Li<sub>4</sub>SiO<sub>4</sub> or Na<sub>2</sub>ZrO<sub>3</sub> [19–23], then their use as CO<sub>2</sub> source could allow the recycling of degraded absorbents after long operation periods. Also, the use of CO<sub>2</sub> and H<sub>2</sub> storage materials eases transportation and storage. Finally, the reduction of inorganic carbonates reinforces the aim of reusing CO<sub>2</sub> as a feedstock in other chemical processes [24–26]. However, despite the recent advances reported in the current literature, the light carbonates-hydrides mixtures have been poorly explored.

In this work, Li<sub>2</sub>CO<sub>3</sub> and MgH<sub>2</sub> were chosen, for the first time to the best of our knowledge, as CO<sub>2</sub> and H<sub>2</sub> portable storage materials to evaluate the direct methanation reaction promoted by

high-energy mechanochemical activation. Specifically, the selection of Li<sub>2</sub>CO<sub>3</sub> gives the possibility to reuse final products obtained from deteriorated CO<sub>2</sub> absorbents. In addition, the formation kinetics of both CH<sub>4</sub> and H<sub>2</sub> was investigated using theoretical models to fit the time-dependent experimental conversion data. In order to clarify the reaction mechanism of the MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> reaction system, a combination of different techniques for structural, microstructural and chemical characterization of the solids was used and complemented by thermodynamic calculations.

## 2. Experimental

### 2.1. Materials preparation

Commercial MgH<sub>2</sub> (Rockwood Lithium, 99.8 %) and Li<sub>2</sub>CO<sub>3</sub> (Alfa Aesar, 99 %) powders were used as precursor reagents. Mixtures with different molar ratio of MgH<sub>2</sub>:Li<sub>2</sub>CO<sub>3</sub>, 4:1 and 2:1 were prepared by ball milling (BM). For each mixture, a total amount of 1 g was used, corresponding to 0.59 g MgH<sub>2</sub>-0.41 g Li<sub>2</sub>CO<sub>3</sub> and 0.42 g MgH<sub>2</sub>-0.58 g Li<sub>2</sub>CO<sub>3</sub> for 4:1 and 2:1 M ratio, respectively. The procedure for the mechanical treatment consisted in sealing each reagent mixture in a vial and ball milling by using a Spex mixer/mill model 8000 adapted for milling at different rotation speeds. The vial and the ball used are made of stainless steel. The ball milling conditions were: ball mass to powder mass ratio of 1–4, room temperature, an argon pressure of 0.98 atm and rotation speed of 750, 875, 925 and 1000 rpm. The milling was stopped each 5 min, avoiding temperature increase in the milling system.

Because of the air sensitivity of the powders, sample handling was performed under a high-purity argon atmosphere inside a glove box device (MBraun) with oxygen and water levels below 1 ppm.

### 2.2. Characterization techniques

The structural and morphological properties of the materials were analyzed by X-Ray Powder Diffraction (XRPD) using a Rigaku DMax diffractometer with CuK $\alpha$  radiation tube, Scanning Electron Microscopy (SEM, ZEISS Crossbeam 340 microscope and SEM, FEI Inspect S50) with Energy-Dispersive X-ray Spectroscopy (EDXS) and solid state FTIR (Perkin Elmer Spectrum Series 400). To prevent the sample oxidation during XRPD measurements, an airtight sample holder with Kapton dome was used. A wide peak at lower angle was observed due to kapton contribution. Using the Scherrer equation [27], the crystallite size of the phases before and after milling was calculated using the following peaks: MgH<sub>2</sub> (2 $\theta$ : 27.9°), Mg(OH)<sub>2</sub> (2 $\theta$ : 18.6°), Li<sub>2</sub>CO<sub>3</sub> (2 $\theta$ : 21.3°), MgO (2 $\theta$ : 42.9°) and Mg (2 $\theta$ : 36.6°). Considering that the area of the main peak of each phase is proportional to the amount of that phase in the crystalline sample, estimations of the proportion of X phase respect to the rest of phases all containing Mg were performed. The proportion (P, percent) of MgH<sub>2</sub>, Mg, or MgO in the starting material and after mechanochemical milling were calculated from XRPD measurements, using the following equation:

$$P_X = \frac{I_X}{I_{MgH_2} + I_{MgO} + I_{Mg}} \cdot 100 \quad (6)$$

where X is the specie of interest and I is the integrated intensity of the most intense reflections of MgH<sub>2</sub> (2 $\theta$ : 27.9°), MgO (2 $\theta$ : 42.9°) and Mg (2 $\theta$ : 36.6°).

For the morphological observations and elemental mapping, powder samples were dispersed on a carbon based tape and coated with gold to improve electrical conductivity. In the case of solid-state FTIR spectroscopy measurements, the powders were mixed

with dry KBr and pressed to pellets under air conditions. The presence of carbon-based solids on the final products was investigated by Raman spectroscopy with a confocal microscope (LabRAM HR Evolution Raman microscope) at room temperature using the laser wavelength of 514 nm.

The gaseous phase was followed by gas-chromatography (GC). Hydrogen (H<sub>2</sub>), methane (CH<sub>4</sub>) and other hydrocarbons were detected using both a Perkin Elmer 8500 and a Fisons 8000 apparatus equipped with a flame ionization (FID) and thermal conductivity (TCD) detectors, respectively. Suitable gas standard mixtures were used to quantify the hydrocarbons production during milling at different times. The conversion values ( $\alpha$ ) for the gas products CH<sub>4</sub> and H<sub>2</sub> were calculated as follows:

$$\alpha_{CH_4} = \frac{n_{CH_4}}{n_{CO_2}} \quad (7)$$

$$\alpha_{H_2} = \frac{n_{H_2}}{n_{MgH_2}} \quad (8)$$

where  $n_{CH_4}$ =moles of CH<sub>4</sub> produced,  $n_{CO_2}$ =moles of CO<sub>2</sub> supplied from Li<sub>2</sub>CO<sub>3</sub>,  $n_{H_2}$ = moles of H<sub>2</sub> produced and  $n_{MgH_2}$ =moles of MgH<sub>2</sub> supplied.

### 2.3. Thermodynamic calculations

The equilibrium compositions for MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system as a function of the pressure were calculated using HSC Chemistry Windows, 6.1 version [28]. When all species in a reaction system are given (reactants and products), the software determines the distribution of the products where the Gibbs free energy of the system reaches its minimum at constant temperature. For calculations, H<sub>2</sub>:CO<sub>2</sub> molar ratio of: 4MgH<sub>2</sub>:Li<sub>2</sub>CO<sub>3</sub>; 2MgH<sub>2</sub>:Li<sub>2</sub>CO<sub>3</sub>; 3.64MgH<sub>2</sub>:Li<sub>2</sub>CO<sub>3</sub>:0.36 Mg and 1.82MgH<sub>2</sub>:Li<sub>2</sub>CO<sub>3</sub>:0.18 Mg were taken into account as initial reagents; it was supposed room temperature condition. For these reaction system, the following phases were considered: Ar, CO<sub>2</sub>, H<sub>2</sub>, CO, O<sub>2</sub>, CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>2</sub>H<sub>6</sub> and H<sub>2</sub>O in the gas phase, and Li<sub>2</sub>O, LiOH, Li<sub>2</sub>CO<sub>3</sub>, Li<sub>2</sub>C<sub>2</sub>, MgH<sub>2</sub>, Mg, MgO, Mg(OH)<sub>2</sub>, MgCO<sub>3</sub> and carbon as possible solid products.

## 3. Results

### 3.1. Ball milling of MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system: structural and microstructural analyses

XRPD patterns of the MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system after milling for different times show the structural and microstructural evolution of the solid phases (Fig. 1). For all cases, a broadening of the peaks was observed due to a gradual modification of microstructural features induced by the mechanical processing. For comparison, the structural study of the reagents before milling shows the high crystallinity of MgH<sub>2</sub>, with minor amounts of Mg, and Li<sub>2</sub>CO<sub>3</sub> (Fig. S1A). Independently on the milling time and the rotation speed, a remnant of the reactants MgH<sub>2</sub> and Li<sub>2</sub>CO<sub>3</sub> as crystalline phases as well as free Mg was identified during mechanochemical processing (Fig. 1A). At higher rotation speeds such as 925 rpm, it is possible to recognize the most intense diffraction peaks of MgO at 42.92° and 62.31°. Progressive formation of MgO was confirmed with the increment of the milling time at 1000 rpm (Fig. 1B); simultaneously Li<sub>2</sub>CO<sub>3</sub> and MgH<sub>2</sub> were detected, indicating their incomplete transformation. Other Li-containing phases were not detected with this technique.

The solids obtained after milling of MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> for 720 min using 750 and 1000 rpm were analyzed by FTIR and Raman (Fig. 2). The FTIR results confirm the presence of Li<sub>2</sub>CO<sub>3</sub> phase in both samples (Fig. 2A), in agreement with XRPD technique. The bands at

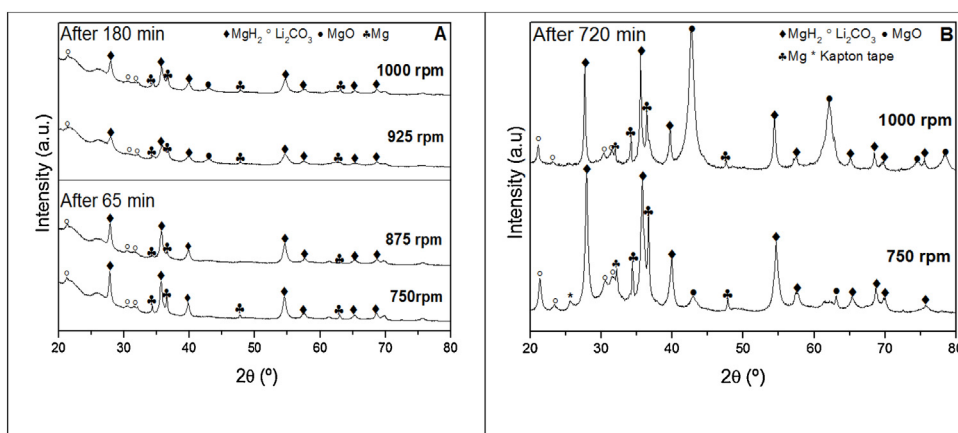


Fig. 1. XRPD patterns after milling of the 4MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system at different milling times (A) and rotation speeds (B).

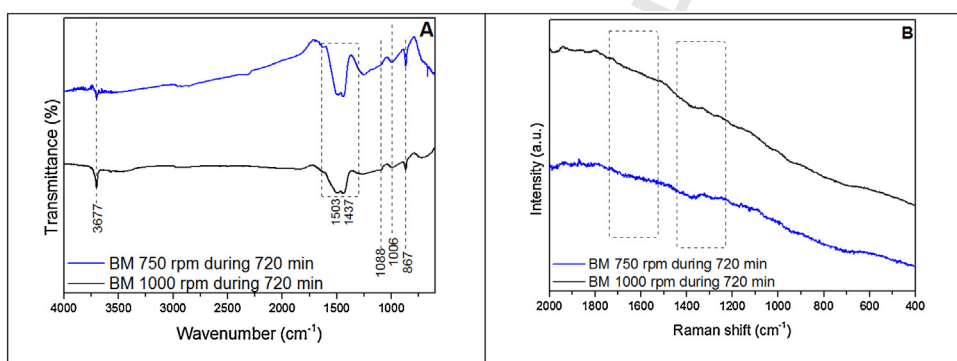


Fig. 2. Solid-state FTIR (A) and Raman spectra (B) of 4MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> after milling at 750 rpm and 1000 rpm during 720 min.

867, 1503 and 1437 cm<sup>-1</sup> due to the bending and asymmetric stretching vibrations of Li<sub>2</sub>CO<sub>3</sub> were observed simultaneously with a small band at 1088 cm<sup>-1</sup> due to the stretching vibration [29]. The band identified at 3677 cm<sup>-1</sup> is related with OH<sup>-</sup> onto Li<sup>+</sup> and it is ascribed to partial hydroxylation of the sample. Its presence can be interpreted as a result of the reaction between Li<sub>2</sub>O with moisture from the air, in agreement with previous work [30]. No evidence of MgO hydroxylation was observed, as it can be inferred by the absence of the stretching vibration at 3699 cm<sup>-1</sup> [31]. This result is in accordance with the minor ΔG° value obtained for hydrolysis of Li<sub>2</sub>O (-88.1 kJ/mol [28]) respect to MgO (-35.7 kJ/mol [28]) at room temperature, suggesting that Li<sub>2</sub>O reacts easily with H<sub>2</sub>O from a thermodynamic point of view.

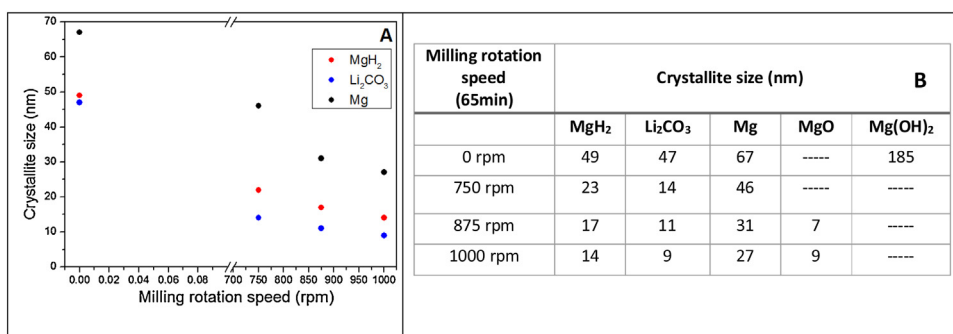
This constitutes an evidence that mechanochemical processing of the MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> mixture for long milling times induces the formation of Li<sub>2</sub>O. In addition, Raman measurements were performed to clarify if amorphous carbon was formed as an intermediate of the reaction, as it was observed in similar systems [18]. The Raman spectra shows the absence of both G and D peaks in the region near 1600 and 1350 cm<sup>-1</sup>, which are ascribed to graphite and defects in carbonaceous solid respectively (Fig. 2B) [32].

The crystallite sizes of the reagents and products were calculated before and after milling using the Scherrer equation (Fig. 3). The values evidence a trend to decrease in grain size with the time and milling rotation speed for the reagents and associated phases (Mg). On the contrary, the phase MgO shows an increment in the grain size during milling probably due to its partial crystallization during mechanical processing.

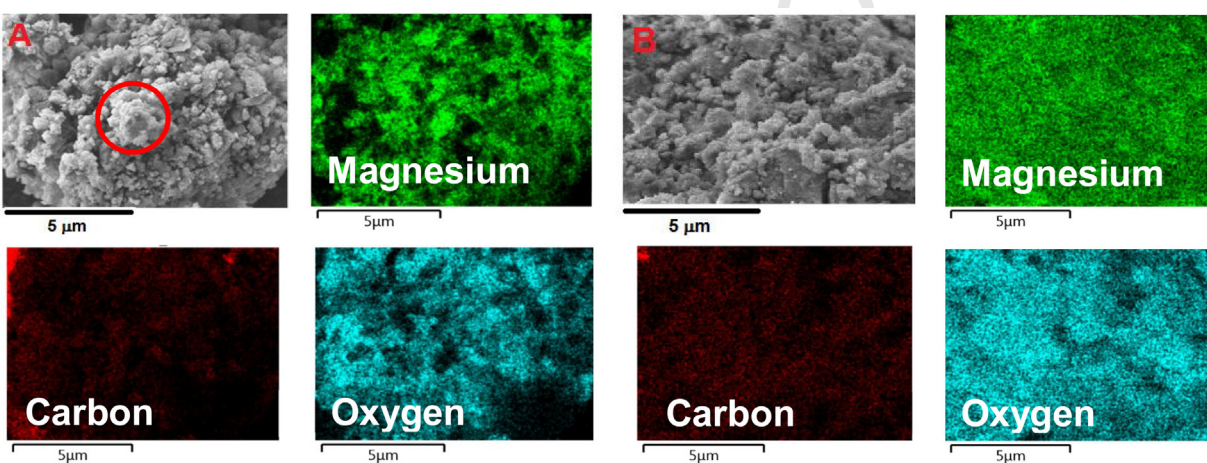
The morphological characterization of starting powders reveals a uniform distribution of MgH<sub>2</sub> agglomerates with an average size of 180 μm, while for Li<sub>2</sub>CO<sub>3</sub> powders display a broad distribution size between 60 and 700 μm (Figs. S1B and S1C, respectively). In both cases, their agglomerates have faceted edges; in particular, partial agglomerate disaggregation was observed for Li<sub>2</sub>CO<sub>3</sub>. Mechanical milling of the MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> mixture introduces relevant morphological modifications in the starting materials. The size distribution of the agglomerates goes from 40 to 60 microns. The as-milled MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> powders at 750 rpm for 65 and 720 min show agglomerates with sponge-type shape (Figs. 4A and B, respectively). The surface of each agglomerate was analyzed by EDXS element mapping evidencing uniform distribution of magnesium, oxygen and carbon due to a well mixing grade of the initial reagents. In particular, after 65 min of milling, there are smooth particles (red circles) with a chemical composition corresponding to Mg. Long times of milling (720 min) favor the uniform distribution of all elements to sizes lower than 1 μm.

### 3.2. Gas evolution during milling: Kinetic analysis of the CH<sub>4</sub> and H<sub>2</sub> production

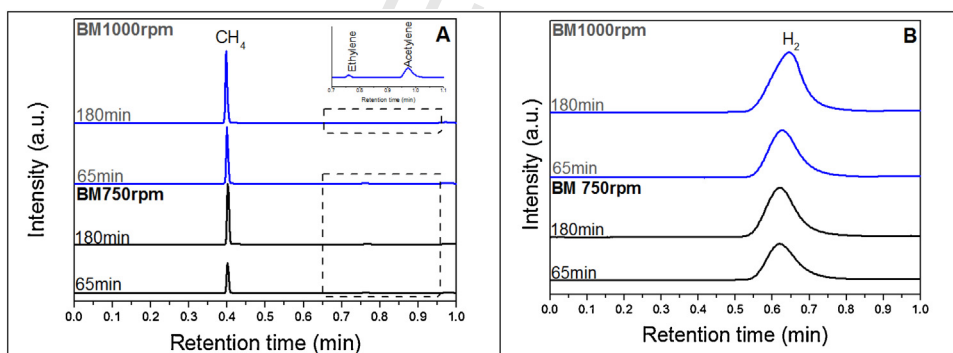
The release of the gaseous species inside the milling chamber was followed by gas chromatography analysis (Fig. 5), taking samples at different reaction times. From short milling times and independently of the energetic conditions, the main products formed by milling of the MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system were methane (Fig. 5A) and hydrogen (Fig. 5B). Signals corresponding to other hydrocarbons such as ethylene and acetylene were found after



**Fig. 3.** Change in the crystallite size as a function of milling rate after 65 min of milling. Plot for the starting reagents (A) and table of all the crystalline species observed (B).



**Fig. 4.** SEM photographs and elemental mapping after milling of the 4MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system at 750 rpm during 65 min (A) and 720 min (B).



**Fig. 5.** Chromatograms of the gas products collected during milling of 4MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system at 750 rpm and 1000 rpm for different times.

milling at 1000 rpm promoted by high-energy milling conditions. The ethylene and acetylene concentrations were below 1 % for all milling rotation speeds. The presence of CO<sub>2</sub> or CO in the gas phase was not detected in any experimental condition.

Evolution of the moles of CH<sub>4</sub> and H<sub>2</sub> as function of milling time at different speeds (Figs. 6A and B) shows that the amounts of CH<sub>4</sub> and H<sub>2</sub> increase with both parameters. The curves of CH<sub>4</sub> show a quadratic dependence with the milling time increase, while H<sub>2</sub> moles grow following an approximately linear behavior from the beginning of the mechanical processing. In both cases, the moles of H<sub>2</sub> formed at a fix milling time and milling rotation speed are at least two times the moles of CH<sub>4</sub> detected.

To study the influence of H<sub>2</sub>:CO<sub>2</sub> molar ratio in the reactivity of the MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system, the most energetic conditions (1000 rpm) were selected to compare the amount of gas produced with the milling time increase (Fig. S2 and Table S1). The shapes of the curves for methane and hydrogen in the plot look similar. In fact, the amount of H<sub>2</sub> (available in the gas phase) increased due to the rise in the H<sub>2</sub>:CO<sub>2</sub> molar ratio and did not have a clear impact on the moles of the CH<sub>4</sub> formed. This result suggests that the mechanism controlling the global process is the same independently of the starting H<sub>2</sub>:CO<sub>2</sub> mol ratio.

To analyze the possible mechanism that controls the reaction between MgH<sub>2</sub> and Li<sub>2</sub>CO<sub>3</sub> during mechanochemical processing,

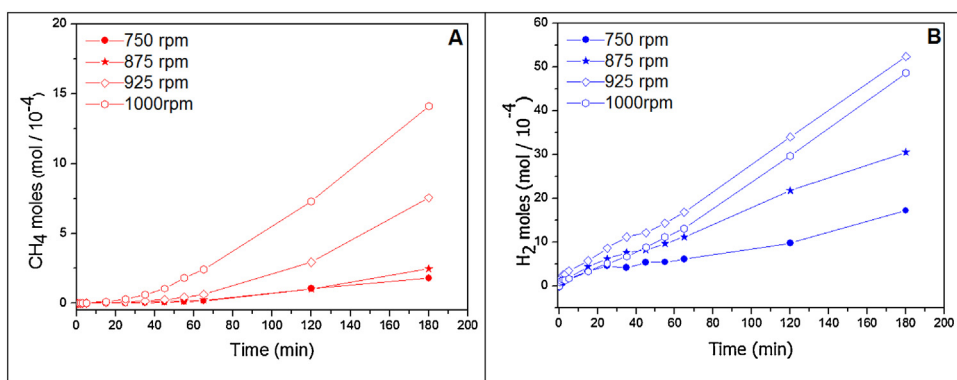


Fig. 6. Moles of CH<sub>4</sub> (A) and H<sub>2</sub> (B) produced during milling of the 4MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system for different milling rotation speeds and milling times.

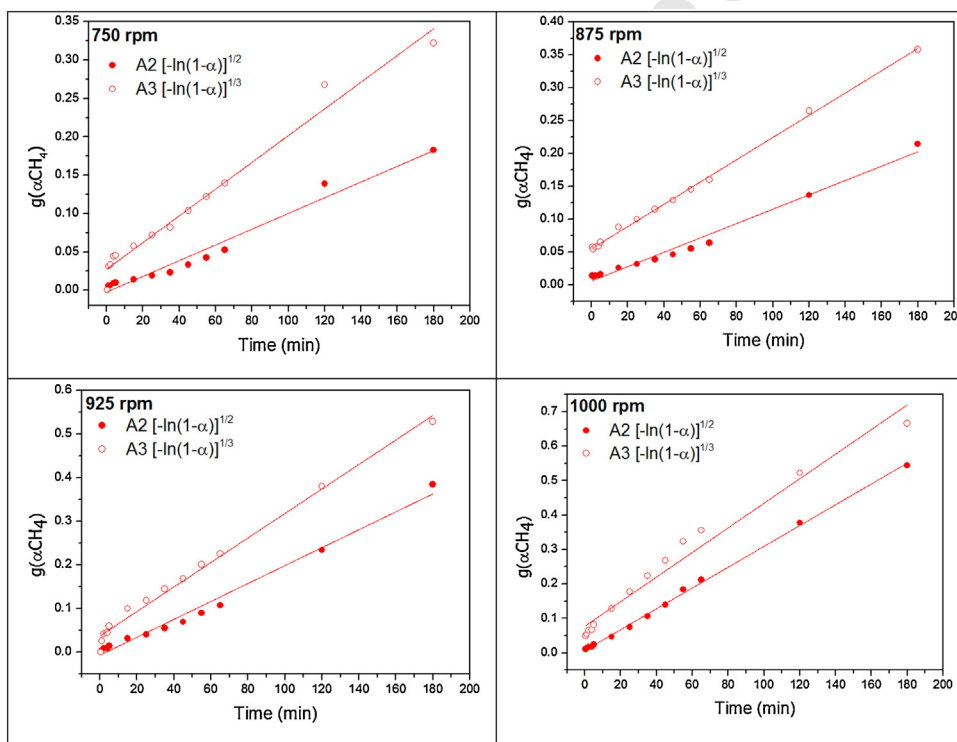


Fig. 7. Fitting of the experimental data for methane conversion using Avrami-Erofev models.

352 the conversion of CH<sub>4</sub> and H<sub>2</sub> was calculated using equations (8),  
353 (9) and data from Fig. 6 (Fig S3). These experimental data were  
354 fitted using theoretical models (Figs. 7 and 8), i.e.  $g(\alpha)$  linearized  
355 functions developed for solid state reaction such as Avrami-  
356 Erofev, Power law and diffusion models (Table 1). These models  
357 assume that the solid-state reaction occurs in a single step;  
358 however, in many cases, intermediate phases are experimentally  
359 observed, indicating a complex reaction mechanism.

360 In this analysis, the value  $R^2$  (squared correlation coefficient)  
361 was chosen as a goodness of fit parameter.  $R^2$  parameter was  
362 obtained by fitting the whole range of milling time (up to 180 min).  
363 The average value of  $R^2$  parameter for each model proposed by  
364 Flanagan et al. [33] is shown in Fig. S4. From this figure it is possible  
365 to notice that the rate controlling mechanism for methane and  
366 hydrogen production is different. The conversion values ( $\alpha$ ) for  
367 methane adjust well with nucleation models such as Avrami-  
368 Erofev and Power law (Fig. 7), with  $R^2$  between 0.97 and 0.998.

369 However, Power law is simply a numerical model without a  
370 specific association with the physical mechanism. In contrast, the  
371 Avrami-Erofev exponent describes the feasibility of nucleation  
372 and usually provides information about the rate-limiting step and  
373 the dimensionality of the growth process.

374 On the other hand, the geometrical contraction models (R2 and  
375 R3) are the most accurate to describe the hydrogen gas formation,  
376 with  $R^2=0.995$  (Fig. 8). These models assume that nucleation  
377 occurs rapidly on the surface of the particle, and all particles are  
378 equivalent in shape and size. The reaction is usually controlled by  
379 the resulting reaction interface progressing toward the center of  
380 the particles.

381 The values of the kinetic rate constant as a function of milling  
382 rotation speed obtained from Figs. 7 and 8 are displayed in Table 2.  
383 The trend shows that the kinetic rate constant for each model  
384 increases with milling rotation speed, showing an enhancement of  
385 the conditions for CH<sub>4</sub> and H<sub>2</sub> gas production.

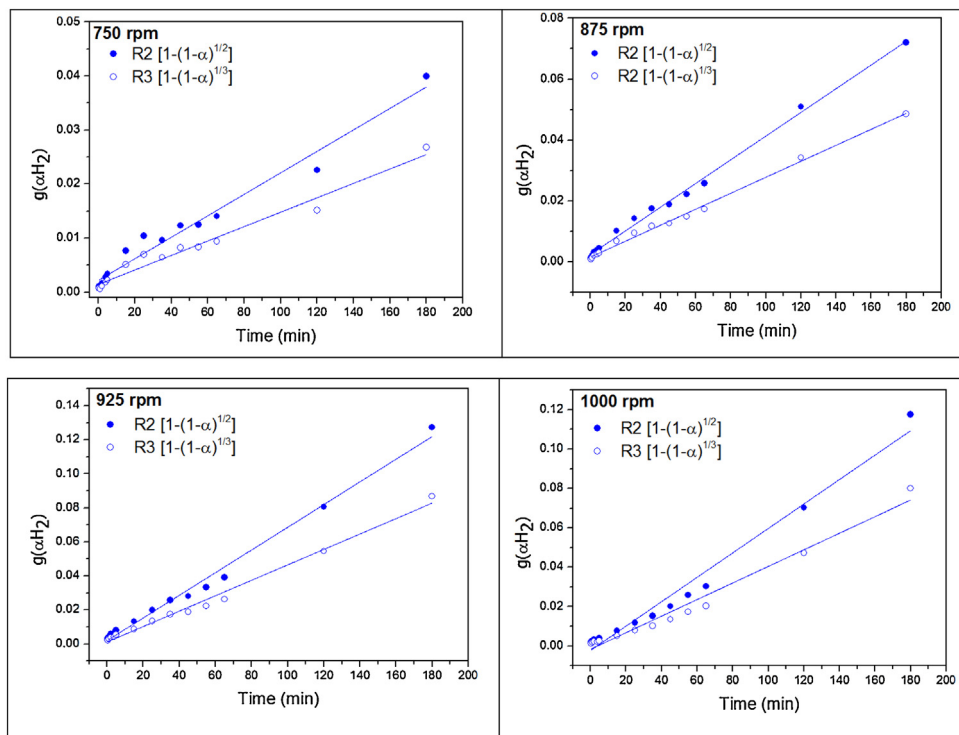


Fig. 8. Fitting of the experimental data for hydrogen conversion using geometrical contraction models.

Table 1

Kinetic models and rate equations used for fitting the conversion of CH<sub>4</sub> and H<sub>2</sub> experimental data.  $\alpha$ =conversion (eqs. 8 and 9),  $k$ =kinetic rate constant,  $t$ =time(s).

Model	Integral form $g(\alpha)=kt$
<b>Nucleation models</b>	
Power law (P2)	$\alpha^{1/2}$
Power law (P3)	$\alpha^{1/3}$
Power law (P4)	$\alpha^{1/4}$
Avrami-Erofeyev (A2)	$[-\ln(1-\alpha)]^{1/2}$
Avrami-Erofeyev (A3)	$[-\ln(1-\alpha)]^{1/3}$
<b>Geometrical contraction models</b>	
Contracting area (R2)	$[1-(1-\alpha)^{1/2}]$
Contracting volume (R3)	$[1-(1-\alpha)^{1/3}]$
<b>Diffusion models</b>	
1D diffusion (D1)	$\alpha^2$
2D diffusion (D2)	$[(1-\alpha)\ln(1-\alpha)] + \alpha$
3D diffusion-Jander equation (D3)	$[1-(1-\alpha)^{1/3}]^2$
<b>Reaction zero-order</b>	
Zero-order (F0)	$\alpha$
First-order (F1)	$-\ln(1-\alpha)$
Second-order (F2)	$(1-\alpha)^{-1}-1$
Third-order (F3)	$0.5[(1-\alpha)^{-2}-1]$

#### 4. Discussion

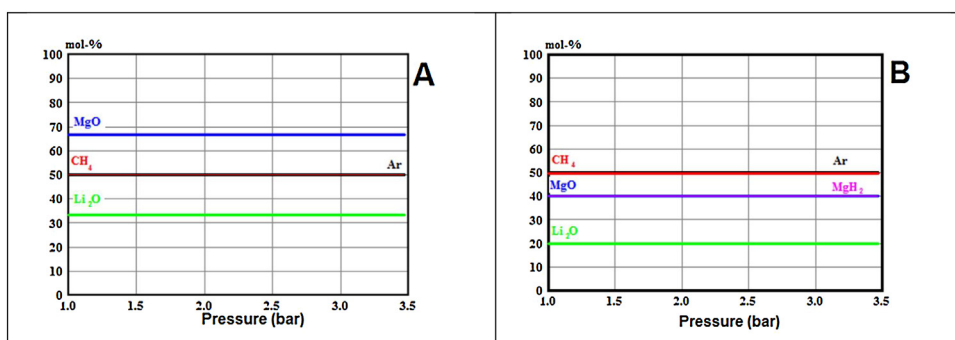
The reaction between MgH<sub>2</sub> and Li<sub>2</sub>CO<sub>3</sub> occurs at room temperature promoted by high-energy milling. Its progress is demonstrated by the gradual formation of both the MgO in the solid phase (Fig. 1) and the mixture CH<sub>4</sub>-H<sub>2</sub> in the gas phase (Fig. 4). As an unexpected result, long milling times (720 min) and high energetic conditions (1000 rpm) are not enough to completely consume the reagents. In fact, both MgH<sub>2</sub> and Li<sub>2</sub>CO<sub>3</sub> starting materials were identified as crystalline phases after reaction under the most energetic conditions (Fig. 1B). Moreover, after a prolonged milling of 720 min, MgH<sub>2</sub>, Mg and MgO are the preponderant phases containing Mg detected by XRPD (Fig. 1); while the presence of LiOH detected by FTIR is an indication of the Li<sub>2</sub>O formation during extended high-energetic milling conditions (Fig. 2B).

The thermodynamic calculations for the MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> system at different H<sub>2</sub>-CO<sub>2</sub> mol ratio (2:1 and 4:1) were performed to determine the equilibrium composition (Figs. 9A and B). These Figures show the equilibrium composition of the gaseous and solid state species as a function of gas pressure at room temperature. Similar results were obtained in both approaches. It can be noted

Table 2

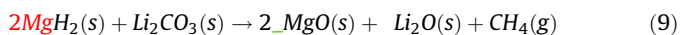
Reaction rate constants obtained for the CH<sub>4</sub> and H<sub>2</sub> formation using Avrami-Erofeyev model and geometrical contraction model, respectively.

Milling rotation speed	Reaction rate constant (s <sup>-1</sup> ), k for CH <sub>4</sub> data	Reaction rate constant (s <sup>-1</sup> ), k for H <sub>2</sub> data
750 rpm	1.66.10 <sup>-5</sup> (A2)	3.3.10 <sup>-6</sup> (R2)
	3.33.10 <sup>-5</sup> (A3)	2.21.10 <sup>-6</sup> (R3)
875 rpm	1.66.10 <sup>-5</sup> (A2)	4.8.10 <sup>-6</sup> (R2)
	3.33.10 <sup>-5</sup> (A3)	4.37.10 <sup>-6</sup> (R3)
925 rpm	3.33.10 <sup>-5</sup> (A2)	1.11.10 <sup>-5</sup> (R2)
	5.10 <sup>-5</sup> (A3)	7.55.10 <sup>-5</sup> (R3)
1000 rpm	5.10 <sup>-5</sup> (A2)	1.0.10 <sup>-5</sup> (R2)
	6.67.10 <sup>-5</sup> (A3)	7.03.10 <sup>-5</sup> (R3)



**Fig. 9.** Equilibrium composition (mol %) as a function of pressure of 2MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> (A) and 4MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> (B).

that MgO and Li<sub>2</sub>O are stable in the condensed phase in the entire range of pressure investigated, while CH<sub>4</sub> appears as the only product in gas phase (Fig. 9). The equilibrium composition of these phases was constant and independent of the total gas pressure of the system at room temperature. As it was seen for MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> with 2:1 ratio, whole oxidation of MgH<sub>2</sub> to MgO is predicted (Fig. 9A), while for 4:1 ratio, free MgH<sub>2</sub> remains without reacting (Fig. 9B). The global reaction based on these thermodynamic calculations can be expressed for the 2:1 ratio as:



In the case of the 4:1 ratio, it is expected the presence of 2 mol of unreacted MgH<sub>2</sub> in the solid products. For thermodynamic calculations performed considering that the starting MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> mixture contains a molar ratio minor than 2:1 or 4:1 due to partial decomposition of MgH<sub>2</sub> to Mg in the starting mixture (Figs. S5A and S5B, respectively), the formation of C or Li<sub>2</sub>C<sub>2</sub> was predicted. From Raman measurements no evidence of the appearance of C (bands at about 1580 and 1340 cm<sup>-1</sup>) and/or Li<sub>2</sub>C<sub>2</sub> (band at 1873 cm<sup>-1</sup>, [34]) was obtained.

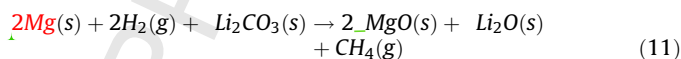
The formation of H<sub>2</sub> in the gas phase was not predicted from thermodynamic calculations independently of the starting MgH<sub>2</sub>:Li<sub>2</sub>CO<sub>3</sub> molar ratio (Figs. 9 and S5). Its detection during milling of the MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> mixture (Fig. 5) could be related with some kinetic restrictions operating in the reaction system, which hinder its consumption to form CH<sub>4</sub>. In fact, the amount of H<sub>2</sub> available in gas phase exceeds the necessary quantity to produce an extra amount of CH<sub>4</sub> (Fig. 6), suggesting that its availability is not a limiting factor. Milling of pure MgH<sub>2</sub>, using the same experimental mechanochemical conditions applied to the 2MgH<sub>2</sub>-Li<sub>2</sub>CO<sub>3</sub> mixture, demonstrates that H<sub>2</sub> is formed by direct MgH<sub>2</sub> decomposition (Fig. S6):



In contrast, no evidence of CO or CO<sub>2</sub> formation was observed after milling pure Li<sub>2</sub>CO<sub>3</sub>. Moreover, when MgH<sub>2</sub> was milled simultaneously with Li<sub>2</sub>CO<sub>3</sub> in the same experimental conditions, H<sub>2</sub> release is promoted (Fig. S6) from the beginning of the reaction. Among the possible reasons, one is that the presence of a second phase with different mechanical properties (Li<sub>2</sub>CO<sub>3</sub>) modifies the milling conditions, affecting the energy transfer during fracturing and cold working phenomena of the powders. Other possible explanation is that the presence of Li<sub>2</sub>CO<sub>3</sub> modifies the stability of MgH<sub>2</sub> by superficial oxidation and favors its decomposition.

Reaction (10) explains the presence of H<sub>2</sub> measured by GC but not envisaged from thermodynamic calculations. As it was previously shown, the amount of H<sub>2</sub> formed exceeds at least in a factor of 2 that corresponding to CH<sub>4</sub> (Fig. 6). According to kinetic studies (Fig. 8), the hydrogen release is controlled by the reaction

interface between MgH<sub>2</sub>/Mg or MgH<sub>2</sub>/MgO. The formation of Mg via reaction (10) allows its reaction with Li<sub>2</sub>CO<sub>3</sub> to produce CH<sub>4</sub> in a H<sub>2</sub> rich environment:



Reaction (11) is thermodynamically favored at room temperature [34]. The combination of reactions (10) and (11) gives the global reaction (9), predicted from thermodynamic calculations. Considering that rate constant for the contracting volume is proportional to the rate constant of the interface-controlled reaction and inversely proportional to the particle length [35], the increment in the rate constant with the milling rotation rate (Table 2) can be attributed to the improvement of the microstructure refinement of the Mg based phases (Figs. 3 and 4).

Considering that reaction (10) is a fast process and that it does not control the global reaction rate, reactions (9) and (11) could occur simultaneously to produce CH<sub>4</sub>. An inspection of the relative change of the MgH<sub>2</sub> and Mg amounts with the milling time for 750 rpm and 1000 rpm (Table S2) shows that the amount of MgH<sub>2</sub> decreases, while the Mg amount increases. This behavior demonstrates that reaction (10) is actually occurring, justifying the detection of H<sub>2</sub> in the gas phase and the increment in the relative amount of Mg with the milling time. In addition, the amount of MgH<sub>2</sub> decreases due to its consumption by direct reaction (9) or combination of reactions (10) and (11). The formation of CH<sub>4</sub> seems to be kinetically restricted by the high stability observed for Li<sub>2</sub>CO<sub>3</sub> under mechanochemical processing. In fact, experimental results demonstrate the absence of CO and CO<sub>2</sub> in the gaseous phase as a carbon source. Moreover, no alternative carbon source in the solid phase, such as amorphous carbon or Li<sub>2</sub>C<sub>2</sub>, were detected (Figs. 1 and 2). Then, kinetic constrains for CH<sub>4</sub> production involve the formation of Li<sub>2</sub>O and MgO through reaction (9) and/or (11). The transfer of oxygen atoms from Li<sub>2</sub>CO<sub>3</sub> toward two different oxides is necessary and can possibly be the rate-controlling process. In this context, the nucleation and growth models are suitable to describe the reaction mechanism (Fig. 7).

Finally, in this study it was demonstrated for the first time that Li<sub>2</sub>CO<sub>3</sub> and MgH<sub>2</sub> can be used as CO<sub>2</sub> and H<sub>2</sub> sources to effectively produce a CH<sub>4</sub>/H<sub>2</sub> fuel mixture at room temperature (see Fig. 10). All resulting products of the mechanochemical treatment of Li<sub>2</sub>CO<sub>3</sub> and MgH<sub>2</sub> are used: the CH<sub>4</sub>-H<sub>2</sub> mixture as fuels in internal combustion engines /gas turbines; and the Mg-Li oxides as absorbers of CO<sub>2</sub> for the treatment of exhaust gases of a power plant. In the whole cycle process, only MgH<sub>2</sub> is consummated. The new addition of MgH<sub>2</sub> allows starting the cycle again by the reaction with Li carbonate (or Mg carbonate).

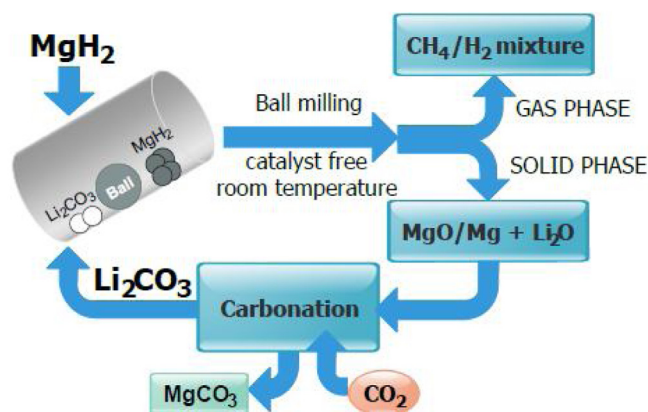


Fig. 10. Schematic representation of the mechanochemical reaction between  $\text{Li}_2\text{CO}_3$  and  $\text{MgH}_2$  and their integration.

By comparison of our mechanochemical processing of  $\text{MgH}_2$ - $\text{Li}_2\text{CO}_3$  with alternative processes to produce  $\text{CH}_4$ , different advantages emerge. Traditional  $\text{CO}_2$  hydrogenation is a process with significant kinetic constraints due to the high stability of  $\text{CO}_2$  molecule. Therefore, it requires the utilization of active and selective catalysts to favor this reaction and produce mainly  $\text{CH}_4$ , avoiding the formation of  $\text{CO}$  as intermediate product. Even though,  $\text{CO}_2$  hydrogenation involves high temperatures, atmospheric pressure and a  $4\text{H}_2:1\text{CO}_2$  molar ratio [36,37]. Another process involves  $\text{MgH}_2$  to reduce  $\text{CO}_2$  without the use of catalysts, but requires 48 h at  $450^\circ\text{C}$  [38]. Although mechanochemical reaction between  $\text{MgH}_2$  and  $\text{CO}_2$  gas occurs at room temperature, long milling times (24 h) are required to obtain yields lower (6% and 15% at 450 rpm and 550 rpm, respectively) [16] than those obtained in this work (3 h of milling, yield of 25% at 1000 rpm, Table S1). Reaction of magnesite ( $\text{MgCO}_3$ ) as  $\text{CO}_2$  source with  $\text{H}_2$  needs  $475$ – $505^\circ\text{C}$  for the  $\text{CH}_4$  production, with simultaneous formation of  $\text{CO}$  [26].

Recently, the use of dual function materials for  $\text{CO}_2$  capture and catalytic conversion to  $\text{CH}_4$  allows the temperature to be reduced to about  $200^\circ\text{C}$ , but the use of noble metals is required [39]. Taking advantage of the mechanochemical processing as a simple, efficient and scalable technology, in this work the  $\text{CO}_2$  contained in  $\text{Li}_2\text{CO}_3$  was reduced using  $\text{MgH}_2$  to produce  $\text{CH}_4/\text{H}_2$  fuels at room temperature with high selectivity, avoiding the use of catalyst and/or solvents, minimizing the generation of waste.

## 5. Conclusions

In this work, the production of the  $\text{CH}_4/\text{H}_2$  fuel mixtures by high-energy mechanochemical activation of the  $\text{Li}_2\text{CO}_3$ - $\text{MgH}_2$  system at room temperature was studied for the first time. The products were obtained through a free-catalyst reaction, with high selectivity and using  $\text{Li}_2\text{CO}_3$  and  $\text{MgH}_2$  as solid portable sources of  $\text{CO}_2$  and  $\text{H}_2$ , respectively. The analyses done by X-ray diffraction, FTIR and Raman spectroscopies, electron scanning microscopy and gas chromatography techniques to study the evolution of the  $\text{Li}_2\text{CO}_3$ - $\text{MgH}_2$  system during milling was complemented with thermodynamic calculations. Theoretical calculations predict the complete  $\text{CO}_2$  reduction to  $\text{CH}_4$ , with simultaneous formation of  $\text{MgO}$  and  $\text{Li}_2\text{O}$ . Experimental evidence supports the progressive formation of  $\text{MgO}$ ,  $\text{MgH}_2$  consumption and the appearance of  $\text{Li}_2\text{O}$  when milling time increases. The presence of  $\text{H}_2$  in the gas phase was due to the high  $\text{Li}_2\text{CO}_3$  stability and the consequent kinetic restrictions in the  $\text{CH}_4$  formation. The conversion of  $\text{MgH}_2$ - $\text{Li}_2\text{CO}_3$  to  $\text{CH}_4/\text{H}_2$  mixtures depends on the milling time, rotation speed and  $\text{H}_2/\text{CO}_2$  molar ratio.

The experimental data of  $\text{CH}_4$  and  $\text{H}_2$  conversion were fitted using theoretical kinetic models with  $R^2$  as a goodness of fit parameter. The best kinetic model for describing the  $\text{CH}_4$  evolution was found to be the JMA (Johnson-Mehl-Avrami) model. It can be associated with  $\text{MgO}$  and  $\text{Li}_2\text{O}$  nucleation and their three-dimensional growth along the interface between  $\text{Li}_2\text{CO}_3$  and  $\text{Mg}/\text{MgH}_2$ . In the case of  $\text{H}_2$  release, the contracting volume model fits very well the experimental data and the process is controlled by the reaction interface between  $\text{MgH}_2/\text{Mg}$  or  $\text{MgH}_2/\text{MgO}$ .

Therefore, the combination of carbonates and metal hydrides are promising portable systems for the *in situ* preparation of  $\text{CH}_4/\text{H}_2$  mixture fuels. The use of  $\text{Li}_2\text{CO}_3$  as a  $\text{CO}_2$  source allows for recycling exhausted absorbents from the post-combustion technologies and to reuse  $\text{CO}_2$  efficiently producing *in situ* fuels with high added value. Currently we are developing alternative methods and innovative explorations to improve the rate of the aforementioned reactions, keeping selectivity and the mild experimental conditions.

## CRediT authorship contribution statement

**María L. Grasso:** Data curation, Validation, Visualization, Formal analysis, Investigation, Writing - original draft. **Luisa Fernández Albanesi:** Data curation, Validation, Investigation, Writing - review & editing. **Sebastiano Garroni:** Conceptualization, Methodology, Investigation, Writing - review & editing, Supervision. **Gabriele Mulas:** Conceptualization, Methodology, Investigation, Writing - review & editing, Supervision. **Fabiana C. Gennari:** Conceptualization, Methodology, Investigation, Writing - original draft, Writing - review & editing, Supervision.

## Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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## Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:<https://doi.org/10.1016/j.jcou.2020.101209>.

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